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EFFECTS OF SPACECRAFT INTERFERENCE ON A 136 MHz PCM TELEMETRY DATA LINK

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**EFFECTS OF SPACECRAFT INTERFERENCE ON A 136 MHz PCM
TELEMETRY DATA LINK**

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Information Processing Division
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November 1969

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Greenbelt, Maryland**

CONTENTS

	<u>Page</u>
ABSTRACT	iii
I. INTRODUCTION	1
II. SPACECRAFT RFI PREDICTION MODEL	2
III. EVALUATION OF SPACECRAFT RFI	6
A. Description of IPD Data Evaluation System	6
B. OSO-5(F) Tape Sample Analysis	8
C. STADAN Station RFI Report Analysis	17
IV. CORRELATION OF PREDICTED, REPORTED, AND TAPE-OBSERVED SPACECRAFT RFI	26
V. OSO-5(F) 136 MHz TELEMETRY DATA LOST OR DEGRADED	30
VI. CONCLUSIONS	35
REFERENCES	36

ILLUSTRATIONS

<u>Figure</u>	<u>Page</u>
1 Radio Link Parameters for RFI Prediction Program	3
2 Flow Diagram, Spacecraft Interference Prediction Computer Program	4
3 The IPD PCM Tape Evaluation System	7
4 IPD Tape Evaluation Analysis for Ft MYRS OSO-5(F) Tape No. 32	9
5 IPD Tape Evaluation Analysis for SNTAGO OSO-5(F) Tape No. 28	11

ILLUSTRATIONS (Continued)

<u>Figure</u>		<u>Page</u>
6	IPD Tape Evaluation Analysis for SNTAGO OSO-5(F) Tape No. 39	13
7	IPD Tape Evaluation Analysis for MOJAVE OSO-5(F) Tape No. 12	15
8	STADAN-Reported Spacecraft RFI Events in 136.0-136.5 MHz Region for January-July 1969 (7 Months)	19
9	STADAN-Reported Spacecraft RFI Events in 136.50-138.00 MHz Region for January-July 1969 (7 Months)	20
10	Percentage Real-Time and Playback Data Affected by Spacecraft RFI in Fourteen (14) OSO-5(F) Passes	32

TABLES

<u>Table</u>		<u>Page</u>
I	STADAN Station-Reported Spacecraft RFI for AIMP-E (3-Week Period)	21
II	STADAN Station-Reported Spacecraft RFI for IMP-5 (1-Week Period)	22
III	STADAN Station-Reported Spacecraft RFI for OSO-5 (3-Week Period)	23
IV	STADAN Station-Reported Spacecraft RFI for ERS-28 (3-Week Period)	24
V	Summary of Typical Station-Reported Spacecraft Interference in 136 MHz Band	25
VI	Comparison of STADAN Report, ADD Predicted, and IPD Observed OSO-5 Spacecraft RFI Start/Stop Times	27

TABLES (Continued)

<u>Table</u>	<u>Page</u>
VII Correlation of Predicted, Observed, and STADAN-Reported Start/Stop Times for Space- craft-Type RFI	28
VIII Spacecraft Parameters Inputted to OSO-5(F) Spacecraft RFI Prediction Program	29
IX IPD Analysis of OSO-5(F) Magnetic Tapes Containing Lost or Degraded Data	31
X OSO-5(F) Real-Time/Playback Lost/Degraded Data Due to Spacecraft RFI, in 14 Tapes	33
XI Summary of OSO-5(F)* Lost and Degraded Data Due to Spacecraft RFI for One Week Sample of 173 Tapes	34

EFFECTS OF SPACECRAFT INTERFERENCE ON A 136 MHz PCM TELEMETRY DATA LINK

I. INTRODUCTION

The quantity and quality of the data retrieved from a spacecraft-to-earth 136 MHz telemetry link are at times affected by either co-channel or adjacent-channel types of radio-frequency interference (RFI) from similar spacecraft operating within the same frequency band. There are presently about 45 spacecraft, supported by the National Aeronautics and Space Administrations (NASA), Space Tracking and Data Acquisition Network (STADAN), each transmitting in the 136-138 MHz space research band.

The STADAN-supported spacecraft employ both pulse-code modulation (PCM) and pulse-frequency modulation (PFM); reference 1 analyzes the effects of spacecraft-type RFI on the Interplanetary Monitoring Platform (IMP-F) spacecraft 136 MHz PFM system.

This report analyzes typical PCM/PM (phase modulated) data samples, obtained while tracking the Orbiting Solar Observatory OSO-5(F) spacecraft, that were processed by the Information Processing Division (IPD). A total of 14 analog-recorded tapes, covering a 7-day randomly selected interval, were examined for suspected spacecraft-type RFI. These 14 analog tapes were either reported by the STADAN stations (RFI Reports) as having spacecraft-type RFI or predicted by the Advanced Development Division (ADD) using the RFI Prediction Model (Reference 2).

The IPD processed tape samples have been correlated with the STADAN reported and ADD predicted spacecraft RFI; there is good agreement between each of the three areas. Each of these aspects are discussed separately.

A significant amount of spacecraft-type RFI was observed and verified to be in the tapes and is described herein.

II. SPACECRAFT RFI PREDICTION MODEL

Based upon known orbital elements (Reference 3), a given spacecraft's orbit can be predicted several weeks ahead in time with reasonable accuracy; these predictions normally include range and aspect angle referenced to a given earth station. A computer program (Reference 2) was consequently developed that predicts station-received signal power levels, based on predicted range and known link parameters, according to Frii's propagation equation:

$$S = \frac{P_{to} G_{to} G_{ro} \lambda_o^2}{(4 \pi R_o)^2} \quad (1)$$

P_{to} = Spacecraft antenna input power, watts

G_{to} = Spacecraft antenna gain, above isotropic

G_{ro} = Station receiving antenna gain, above isotropic

λ_o = Operating wavelength

R_o = Spacecraft-to-station range (same units as λ_o).

STADAN stations at times experience RFI due to the simultaneous appearance of multiple spacecraft having overlapping 136 MHz emission spectrum. A RFI can result from two or more spacecraft present simultaneously within the main lobe, or from an interfering spacecraft transversing a station's antenna side lobe while the spacecraft being tracked is positioned within the main lobe (see Figure 1).

For a steerable antenna (e.g., 85 foot diameter dish), the spacecraft being tracked is assumed positioned perfectly within the main lobe at the maximum gain point; whereas RFI can appear at any point in the radiation pattern. Both the main lobe and side lobes are input to the computer in one degree increments; the desired power level, S, and interference power level, I, being simultaneously determined at two-minute time intervals. Interference-to-signal ratios, I/S, are then computed from equation (1) for all spacecraft. The magnitude of the predicted I/S ratio is an indication of the amount of spacecraft RFI present, an interference condition being defined as existing when the interference power level, I, is 20 db, or less, below the tracking signal level, S.

The computer flow diagram, for the RFI prediction model, is shown in Figure 2. Also shown is a proposed interfacing of the RFI model into an operational system within the T&DS Directorate. The I/S ratios, values of I and S, are simultaneously printed and identified, for each spacecraft for each time reading.

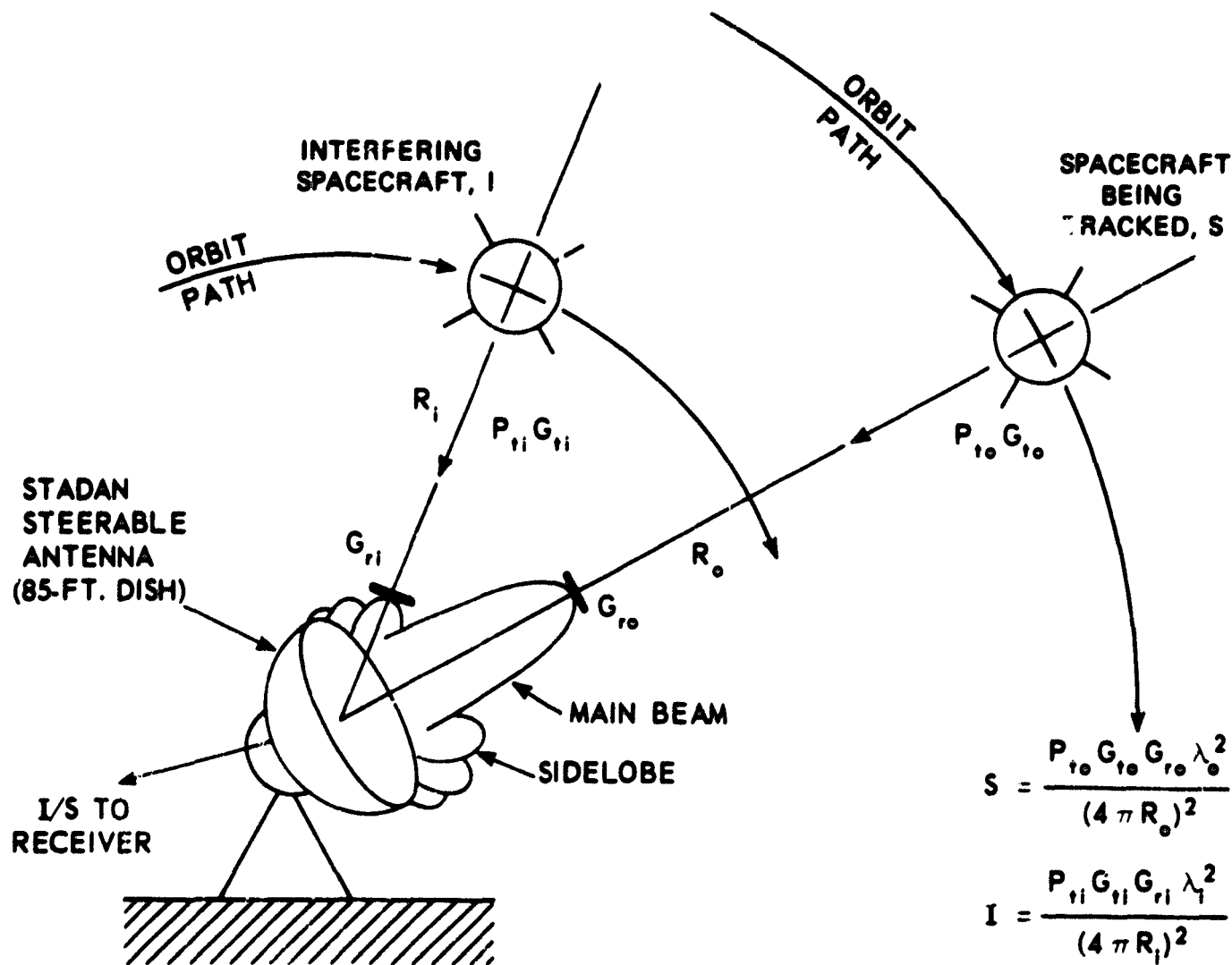


Figure 1. Radio Link Parameters for RFI Prediction Program

Prior to computing the I/S ratio, a spacecraft visibility search sub-routine eliminates spacecraft below a minimum restricted elevation angle (i.e., 10 degrees and below), and a frequency search is made based upon the criteria:

When

$$|f_o - f_i| \leq \frac{B_o}{2} + \frac{B_i}{2}, \quad (2)$$

RFI is present if

$$\frac{I}{S} \geq -20 \text{ db.}$$

STATION DATA:

- GEODETIC COORDINATES
- ANTENNA PATTERNS IN 1° INCREMENTS
- RESTRICTED ELEVATION ANGLES " • 10° & BELOW
- THRESHOLD SENSITIVITY
- 1/5 CRITERION

SPACECRAFT DATA:

- BROUWER MEAN OR NORAD ORBITAL ELEMENTS EPOCH TIME & DRAG TERMS
- TRANSMIT CARRIER FREQUENCY
- SPECTRAL BANDWIDTH
- RF POWER LEVEL

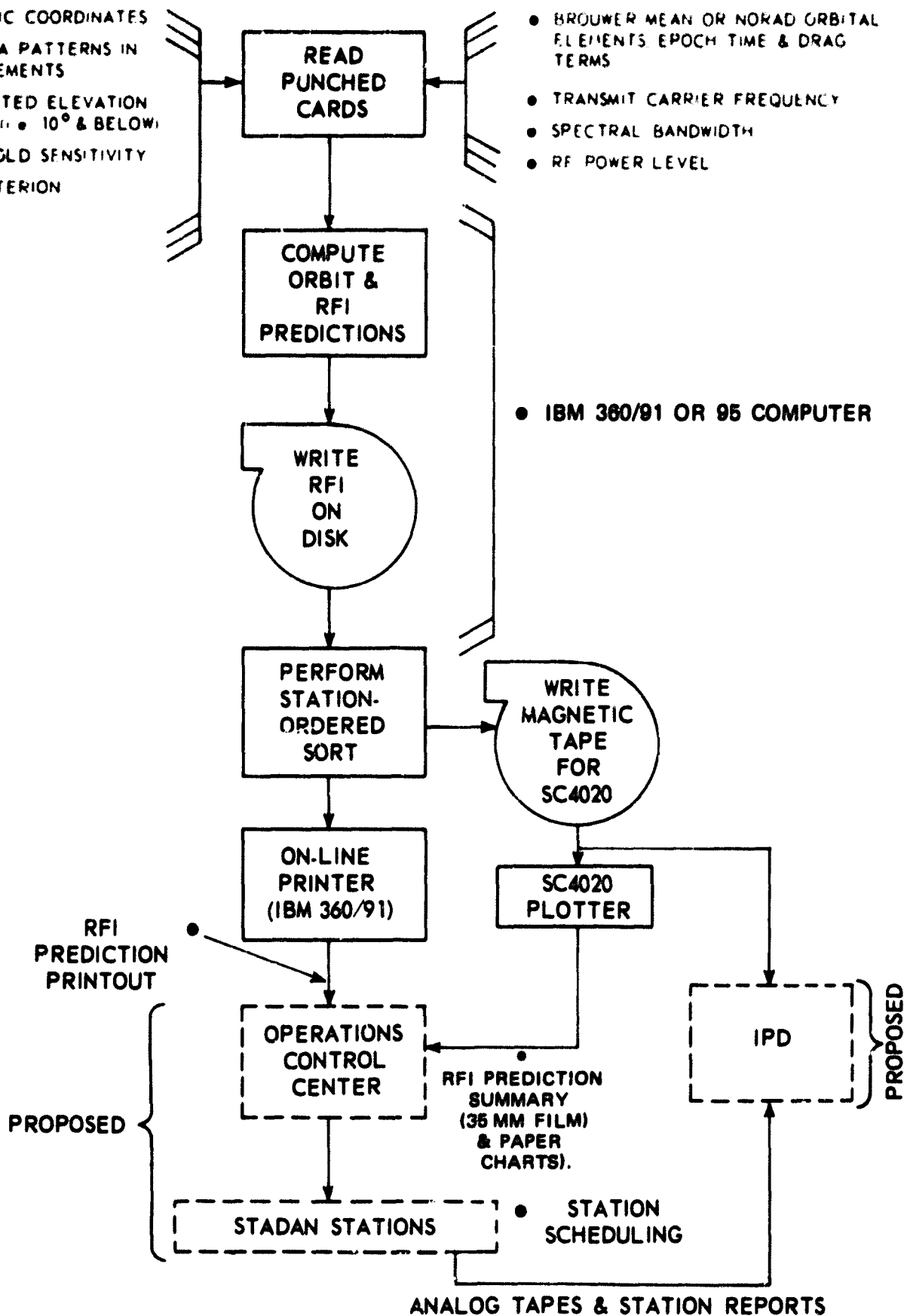


Figure 2. Flow Diagram, Spacecraft Interference Prediction Computer Program

The bandwidths, B_0 and B_i , are the emitted spectral bandwidths of the respective tracking and interfering spacecraft; whereas f_0 and f_i are the respective carrier center frequencies. An ideal, uniformly flat, emitted spectral bandwidth is assumed in order to simplify computations; the spectrum is assumed symmetrically centered about the carrier frequency. The computed signal levels are compared to the station's receiver threshold sensitivity to eliminate weak signals, below threshold, from the printout.

The predicted I/S ratios were computed at 2-minute intervals; I/S ratios then were plotted on the IPD tape evaluation strip charts along with STADAN-station recordings of receiver automatic gain control (AGC). The averaged PCM frame sync correlator output was used to detect the presence of RFI in the OSO-5(F) tape samples. Certain additional ancillary-type data processing equipment, including a spectrum analyzer, was also used to identify spacecraft RFI.

III. EVALUATION OF SPACECRAFT RFI

A. Description of IPD Data Evaluation System

The analog tapes, recorded by STADAN, are mailed to the IPD and generally processed by orbit groups in a chronological order. Those passes which fail to meet established criteria are investigated for anomalies such as those reported by STADAN in the analog tape logs, pass summaries, and daily station reports. In some cases, when the degraded data are unaccountable, the analog tapes are reprocessed. The IPD determines what data are processable from the orbit groups. The ADD is presently developing a system for flagging and identifying potential RFI passes for possible IPD correlation with data quality and data recovery results (Reference 4).

For a more detailed study of signal anomalies, a strip chart analysis is often performed such as shown on Figure 3 for PCM data (Reference 5). This analysis gives a visual indication of any burst-type noise which appears in a pass. A spacecraft RFI unique noise-strip-chart characteristic can be identified. Strip charts were obtained, using the IPD's E-5 tape evaluation line, with the addition of a PCM Performance Monitor, recently developed by the Processor Development Branch, which provides strip chart and quality analyses of various recorded analog signals. The strip chart contains information such as: (1) the receiver AGC recordings, (2) the PCM tape evaluation processor search-to-lock indicator (indication of IPD's data recovery), (3) an average frame sync error rate indicator (indication of IPD's data quality), (4) the bit synchronizer 1/2 bit slippage indicator (indication of jitter), (5) STADAN and IPD's combined ground tape recorder reproduce wow/flutter and drift characteristics, (6) the serial decimal time code, and (7) an indication of the signal plus noise (S + N) amplitude level variations of the "raw" PCM signal.

The performance monitor counts the relative number of frame sync words, recovered with zero bit errors, when the PCM system is in the "lock" mode. The ratio of the number of frames with zero errors in the frame sync word to the number of recovered frames (FOE) is defined as:

$$\text{FOE} = \frac{\text{Number of recovered frame sync words with zero errors}}{\text{Number of recovered frames}} \leq 1 \quad (3)$$

Also,

$$\text{FOE} \approx (1 - n P_e) \quad (4)$$

where

$$\begin{aligned} n &= \text{number of bits in each frame sync word} \\ P_e &= \text{average bit error probability} \leq 1/10 \end{aligned}$$

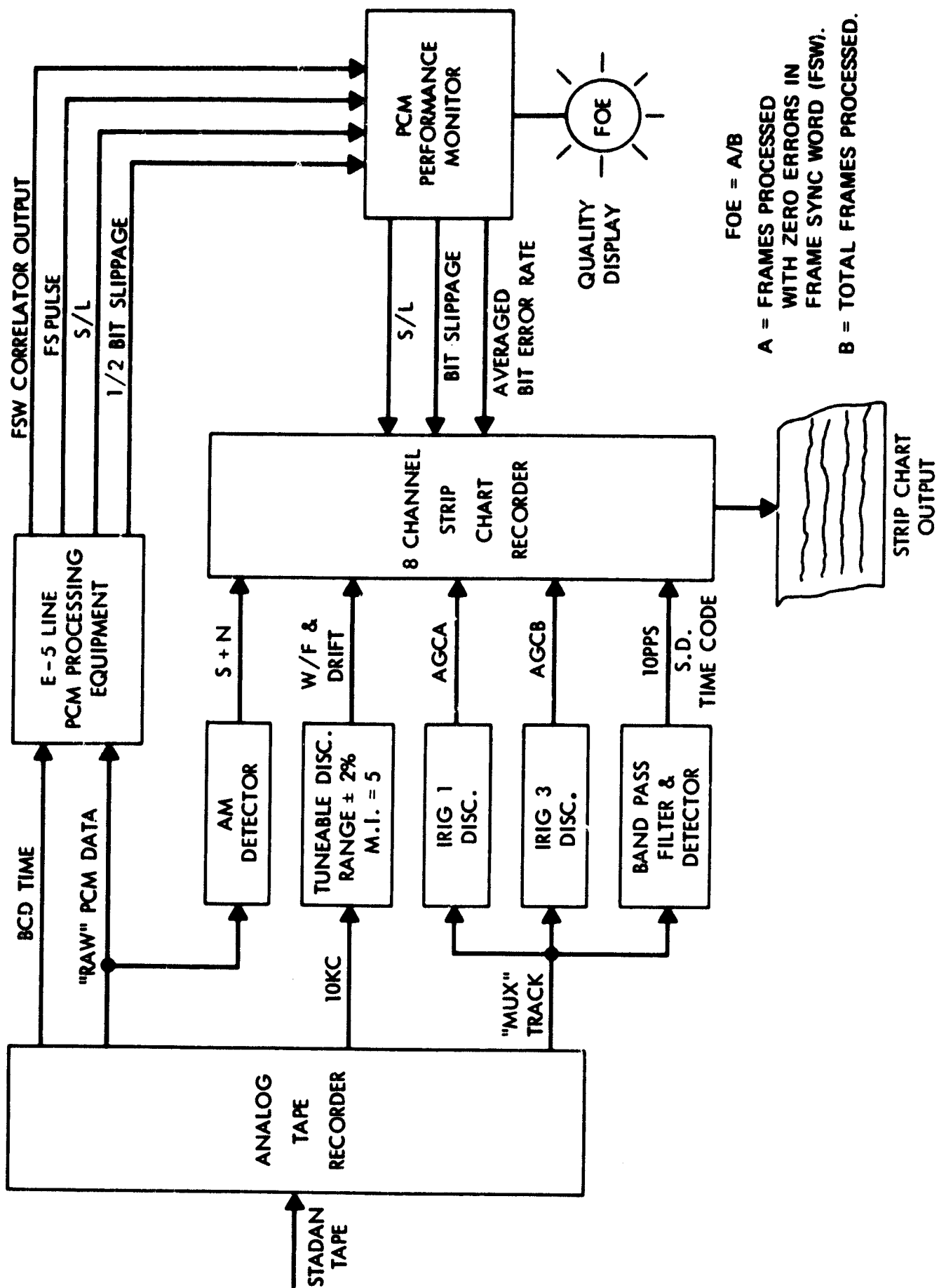


Figure 3. The IPD PCM Tape Evaluation System

In practice, the acronym, FOE, is a figure-of-merit quality factor; the FOE parameter, obtained from the first expression, being used in the second expression to compute the PCM bit-error probability, P_e . It is assumed that the bit errors are independent, and that the process is stationary.

B. OSO-5(F) Tape Sample Analysis

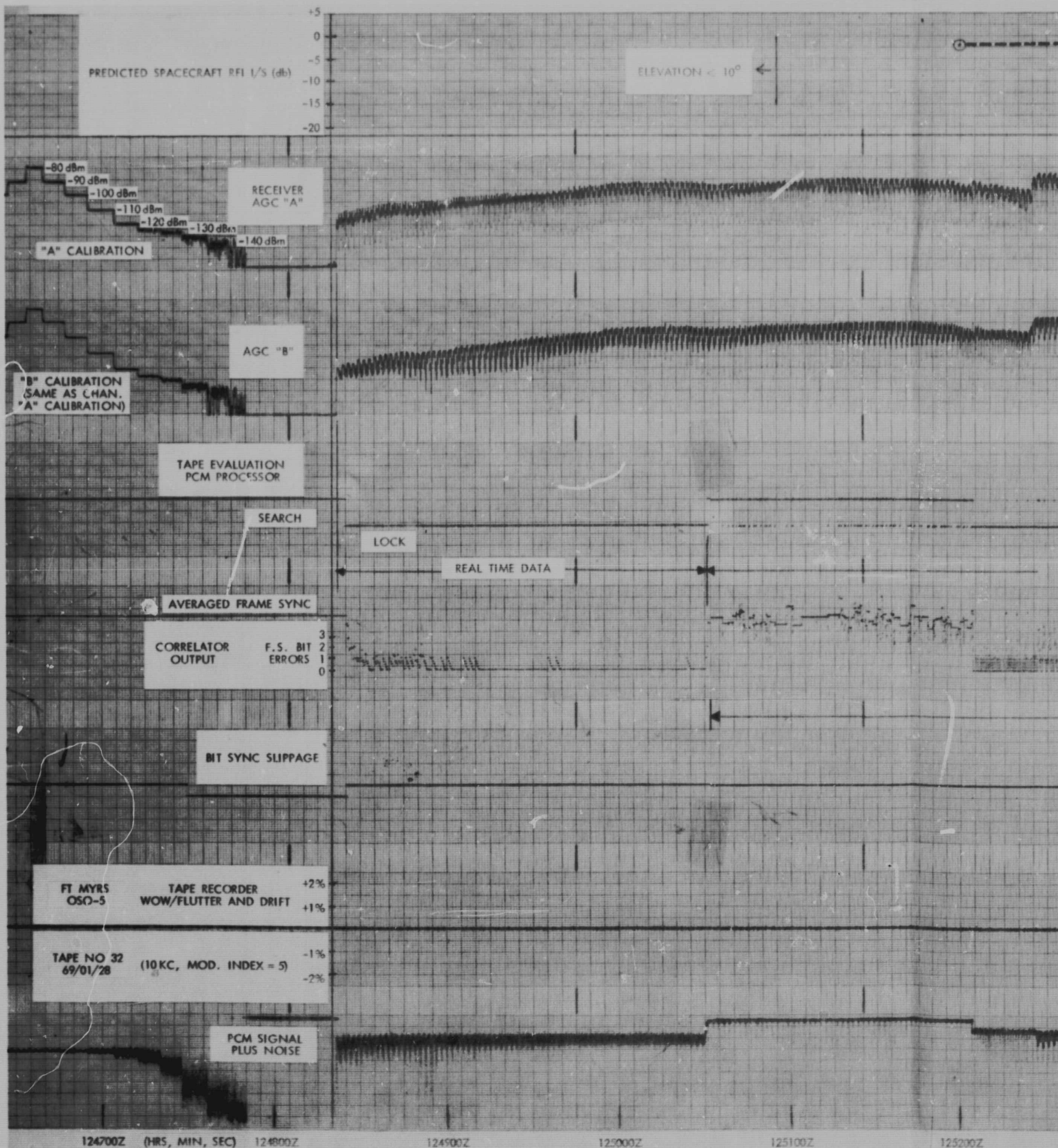
A 7-day period (randomly selected) of OSO-5(F) spacecraft PCM telemetry tapes covering January 26 through February 1, 1969 was examined for spacecraft type RFI. A total of 14 analog tapes (reported by the STADAN stations or predicted by the ADD) were verified by the IPD evaluation system as having various amounts of spacecraft-type RFI.

Four of the 14 OSO-5(F) analog strip-charts were selected for discussion in this report and are shown in Figures 4 through 7, inclusive. Figure 4, corresponding to the Fort Myer's tape No. 32, reveals that a significant portion of a spacecraft pass can be lost, or seriously degraded, 5.5 minutes (42%) of the 13-minute pass being thus affected as observed by the frame sync correlator output channel during the "playback" data mode. It should be noted that the "playback" data was almost completely obliterated in this particular pass. On the other hand, the narrow band "real-time" data mode was affected less than the wide band "playback" data since the "playback" data radio-frequency spectrum is much wider (14.4 kilobit/sec) compared to the "real-time" spectrum with a bit rate of 800 bits/sec. The "playback" mode is therefore more susceptible to adjacent channel RFI than the "real-time" mode. The predicted I/S ratio (top channel, Figure 4) indicates that interference from the OAO-A2 spacecraft, operating on a 136.260 MHz carrier frequency, was sufficiently high ($I/S \geq -20$ db) to interfere with the OSO-5(F) channel, operating on an assigned carrier frequency of 136.290 MHz during the wide band "playback" transmission.

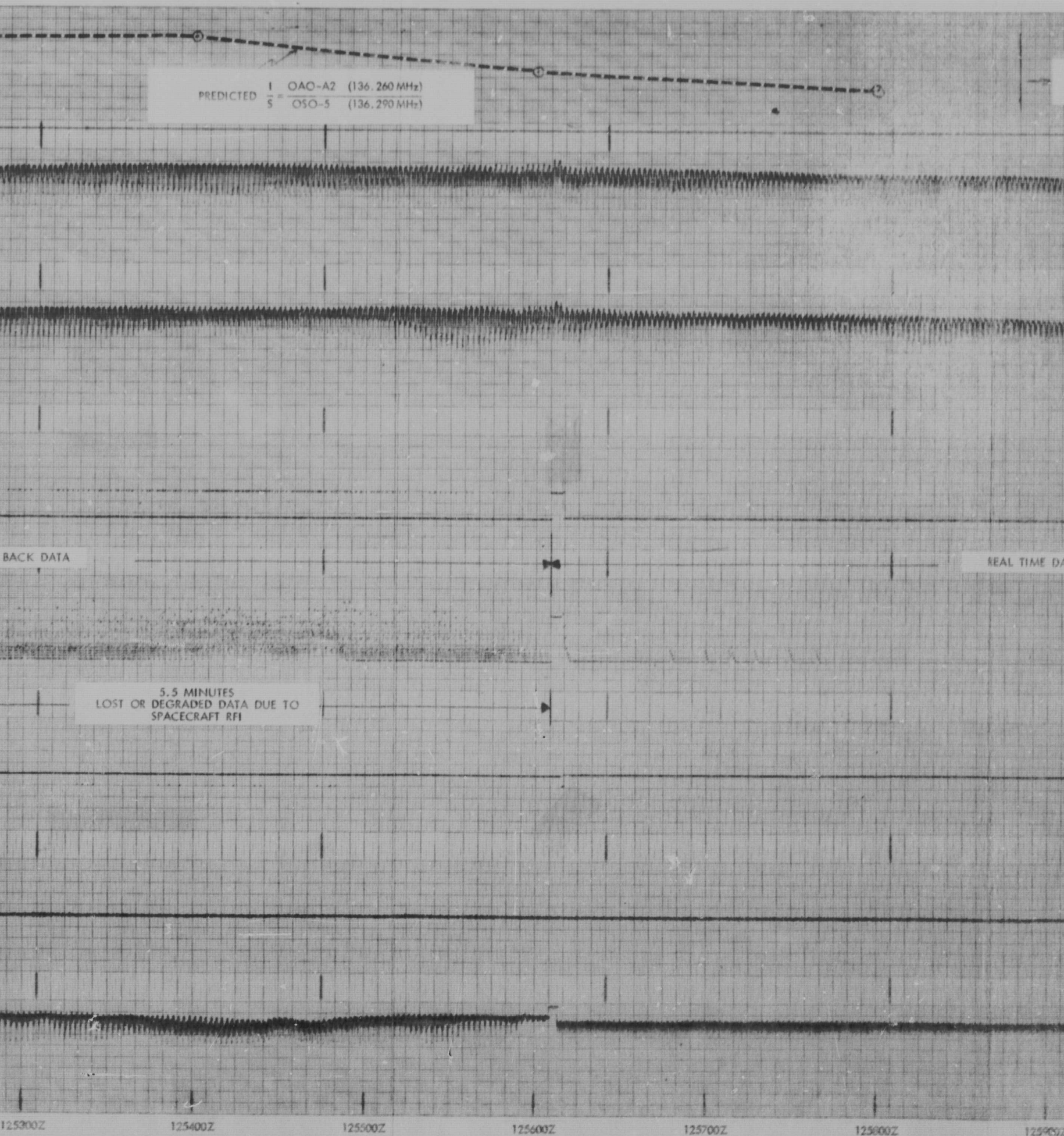
Figure 5, corresponding to the OSO-5 Santiago tape No. 28, shows that the interference appearing in the averaged Frame Sync Correlator Output channel is highly correlated with the predicted interference-to-signal (I/S) ratio.

The receiver channel "B" AGC recording, in Figure 5, shows that the "B" channel was inadvertently phase locked to the interfering OAO-A2 signal, on 136.260 MHz, appearing near the end of the pass; whereas, receiver channel "A" was locked to OSO-5 on 136.290 MHz properly. The IPD clearly identified the interfering OAO-A2 baseband bit rate by analyzing the resulting data beat frequency from the OSO-5 magnetic tape recording. Furthermore, both receiver channels "A" and "B" were inadvertently phased locked to the interfering 136.260 MHz OAO-A2 signal at the beginning of the pass.

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FOLDOUT FRAME #2

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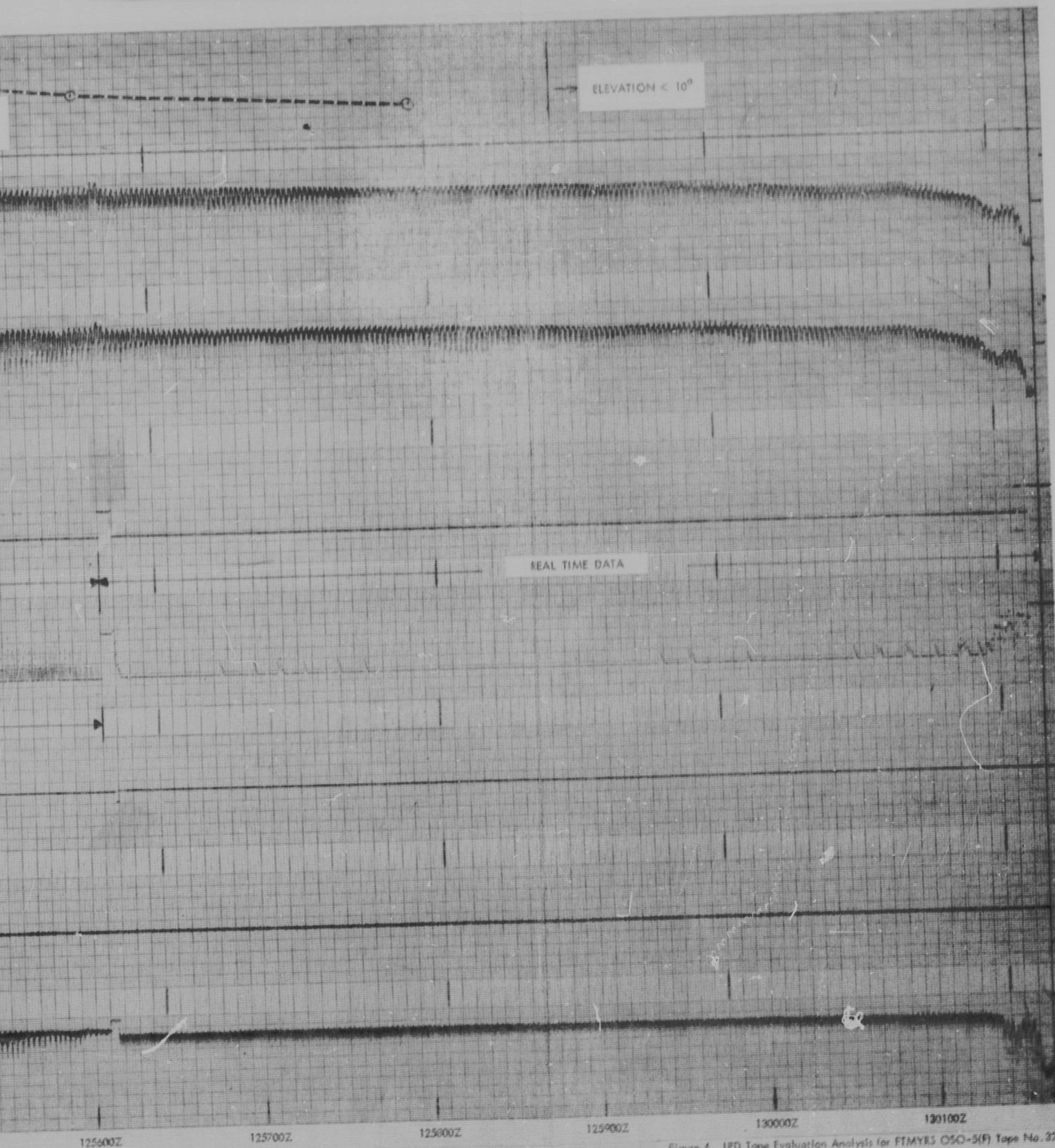
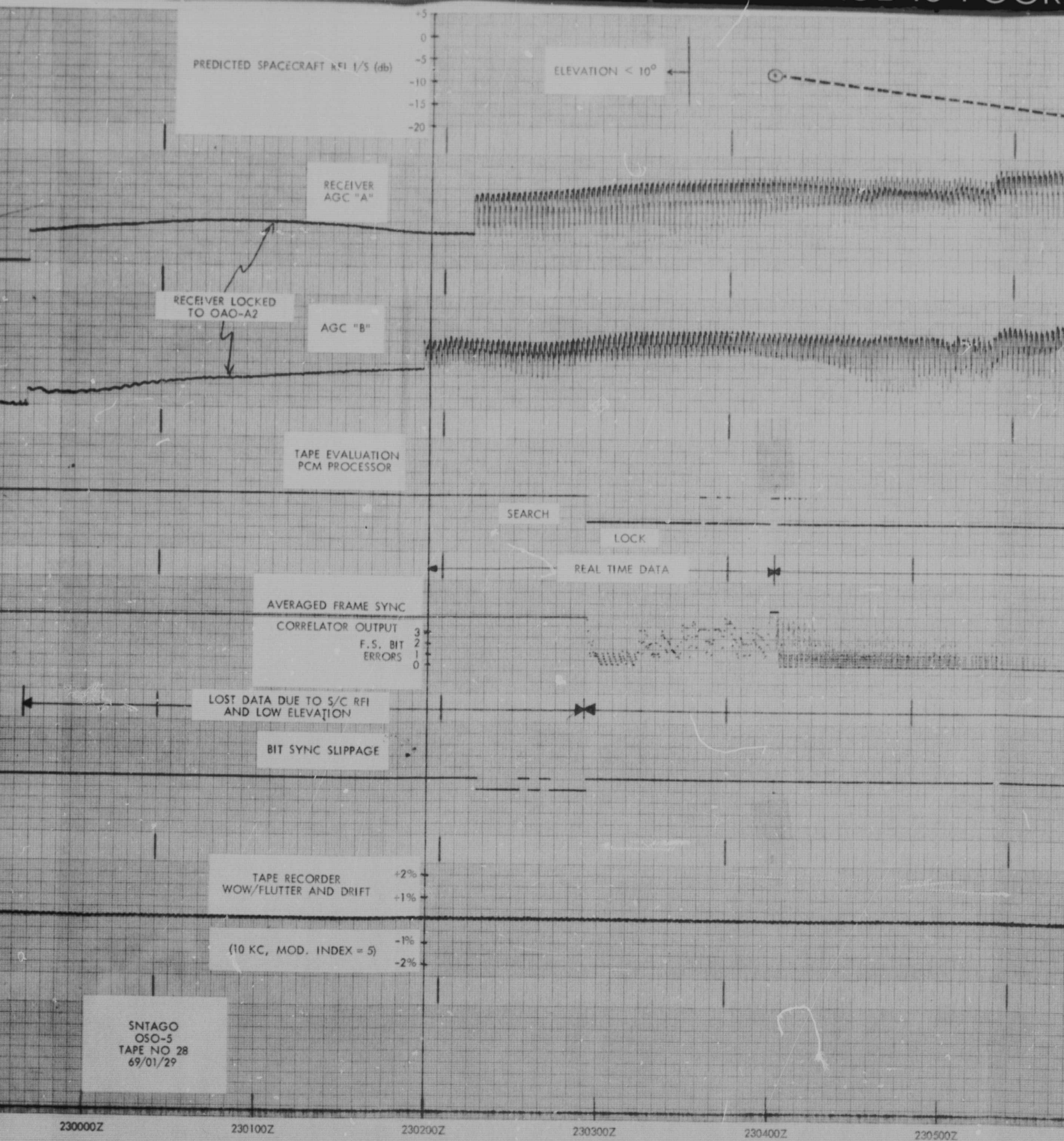


Figure 4. IPD Tape Evaluation Analysis for FTMYR5 OSO-3(F) Tape No. 22

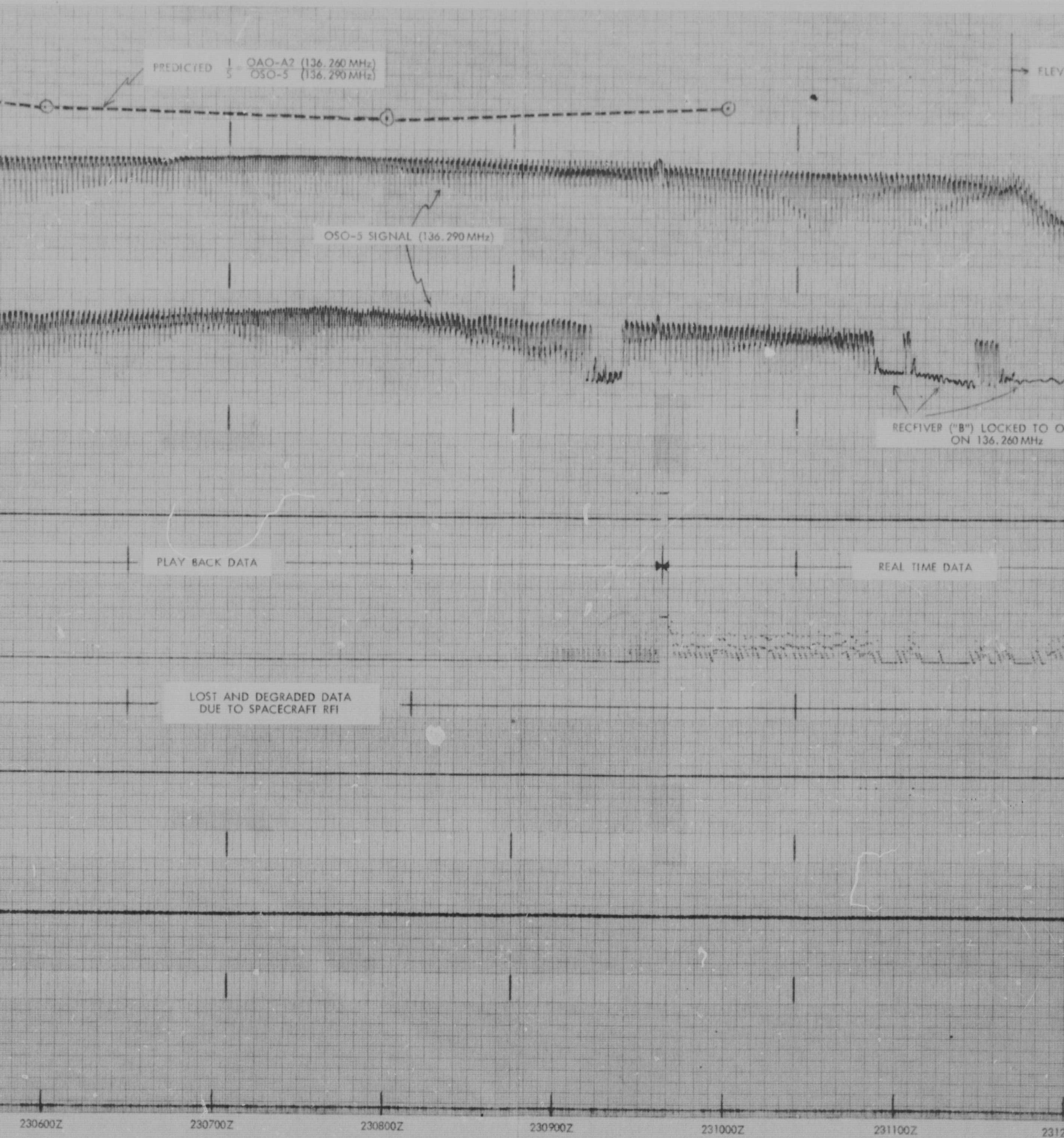
FOLDOUT FRAME #3

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SNTAGO
OSO-5
TAPE NO 28
69/01/29

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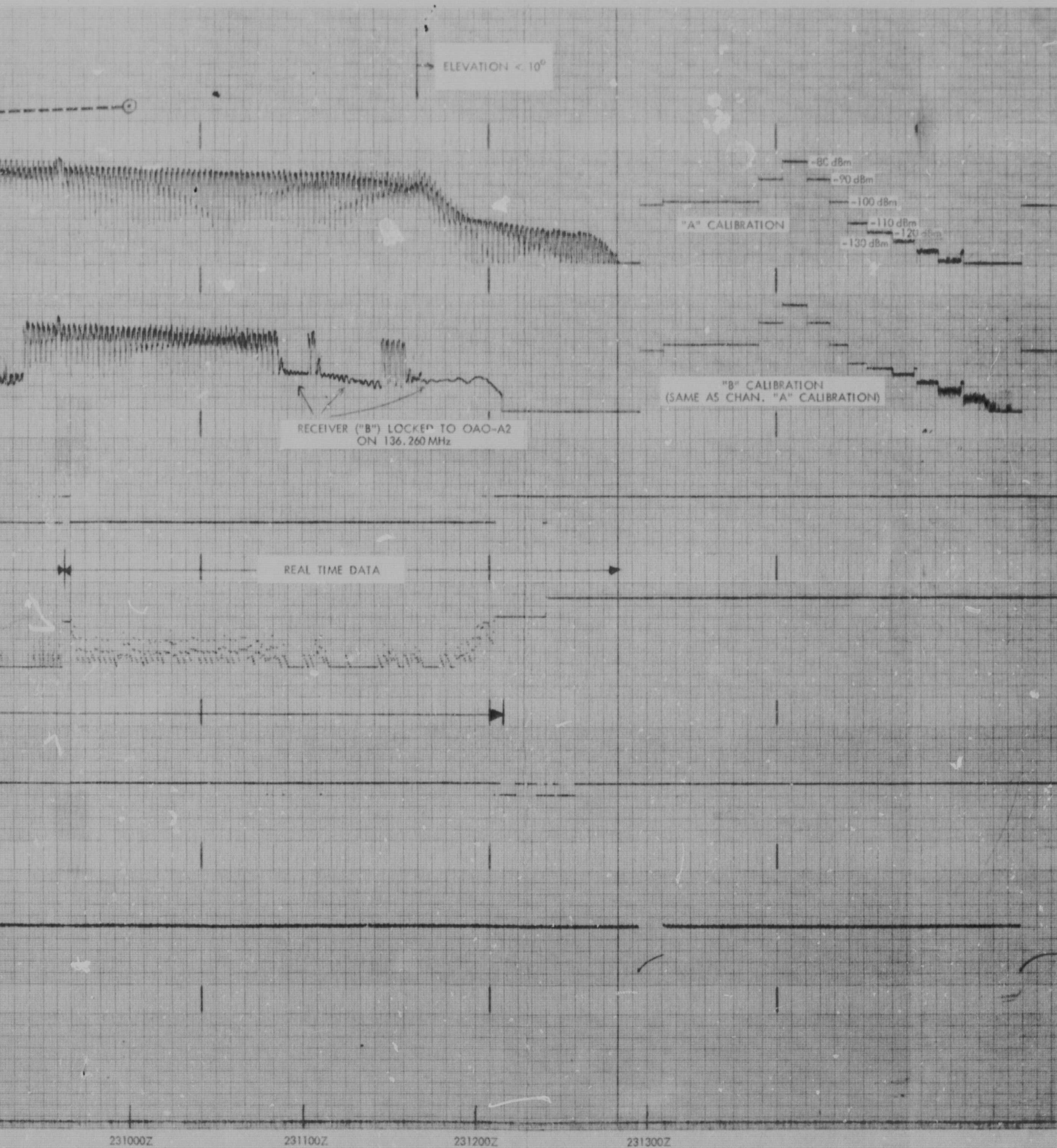
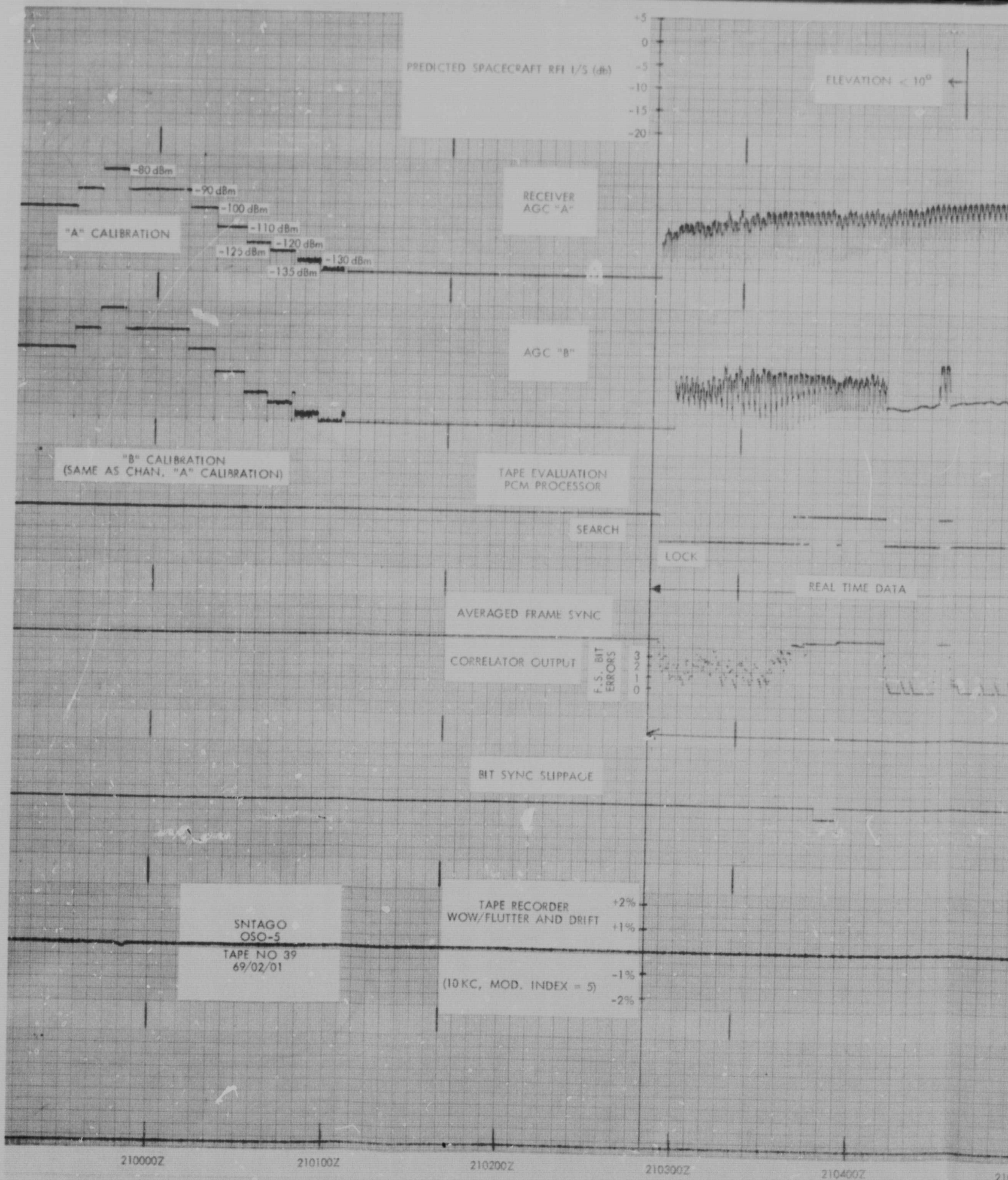


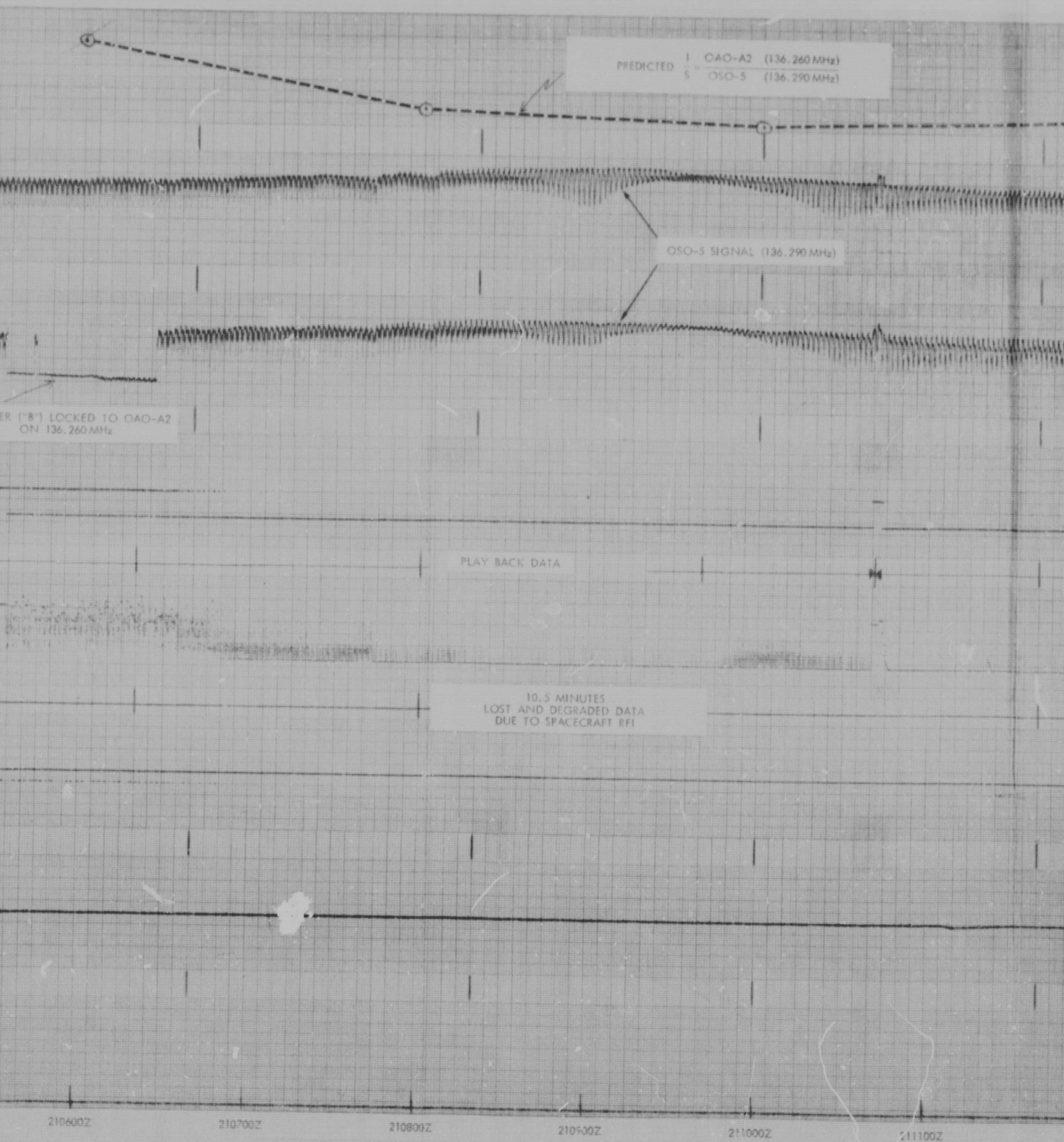
Figure 5. IPD Tape Evaluation Analysis for SNTAGO OSO-5(F) Tape No. 28

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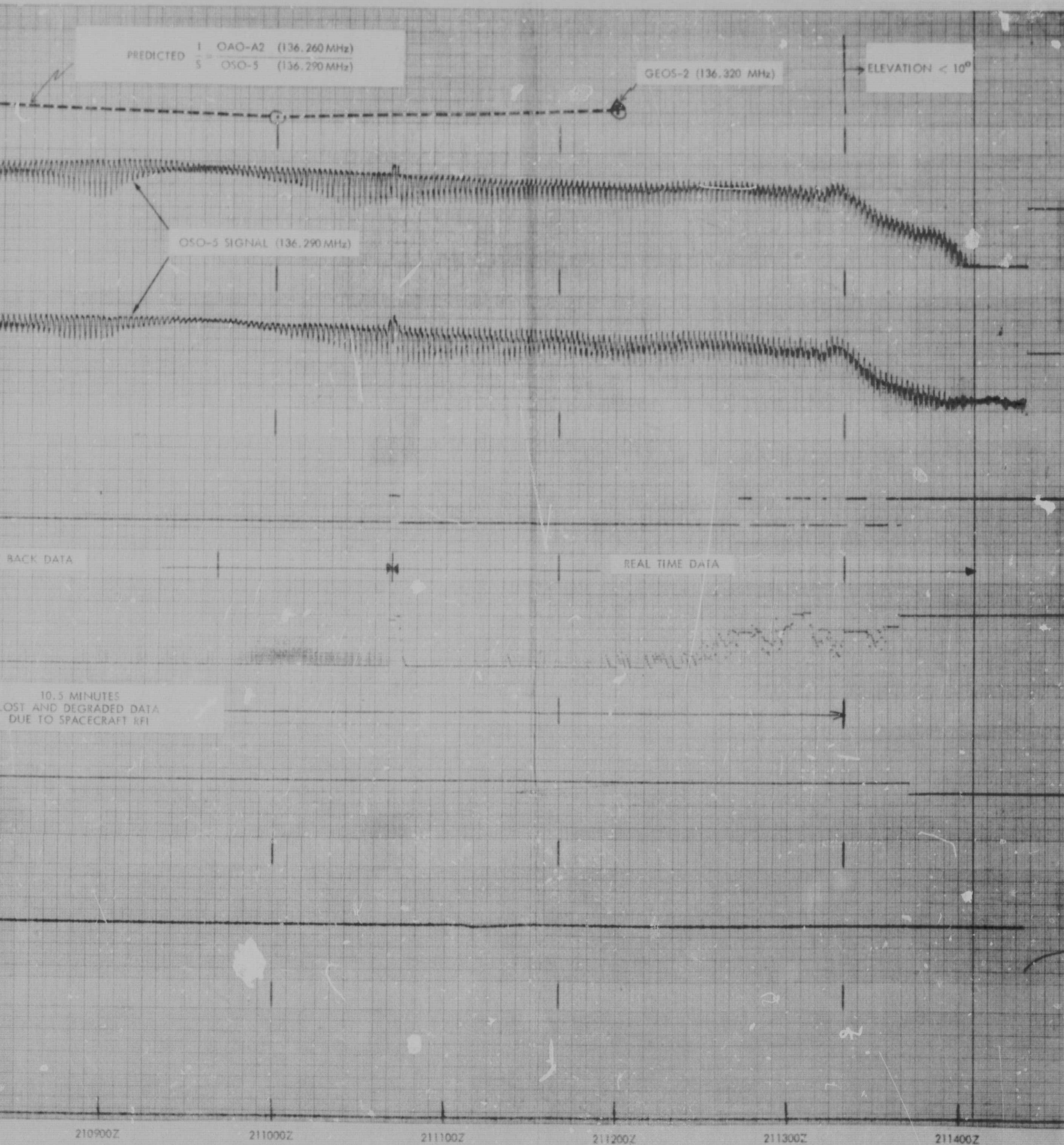
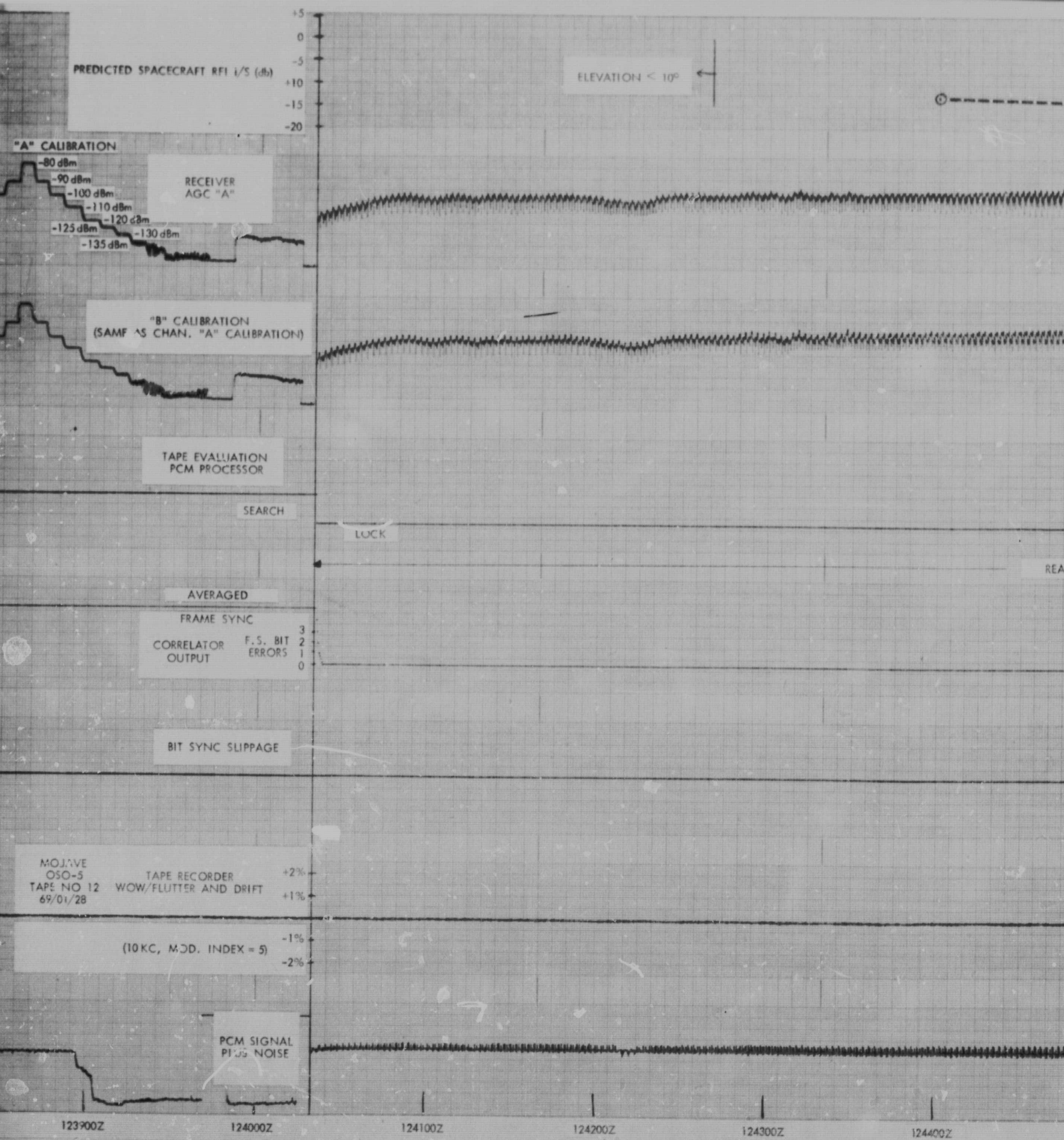


Figure 6. IPD Tape Evaluation Analysis for SNTAGO OSO-5(F) Tape No. 39

FOLDOUT FRAME #2

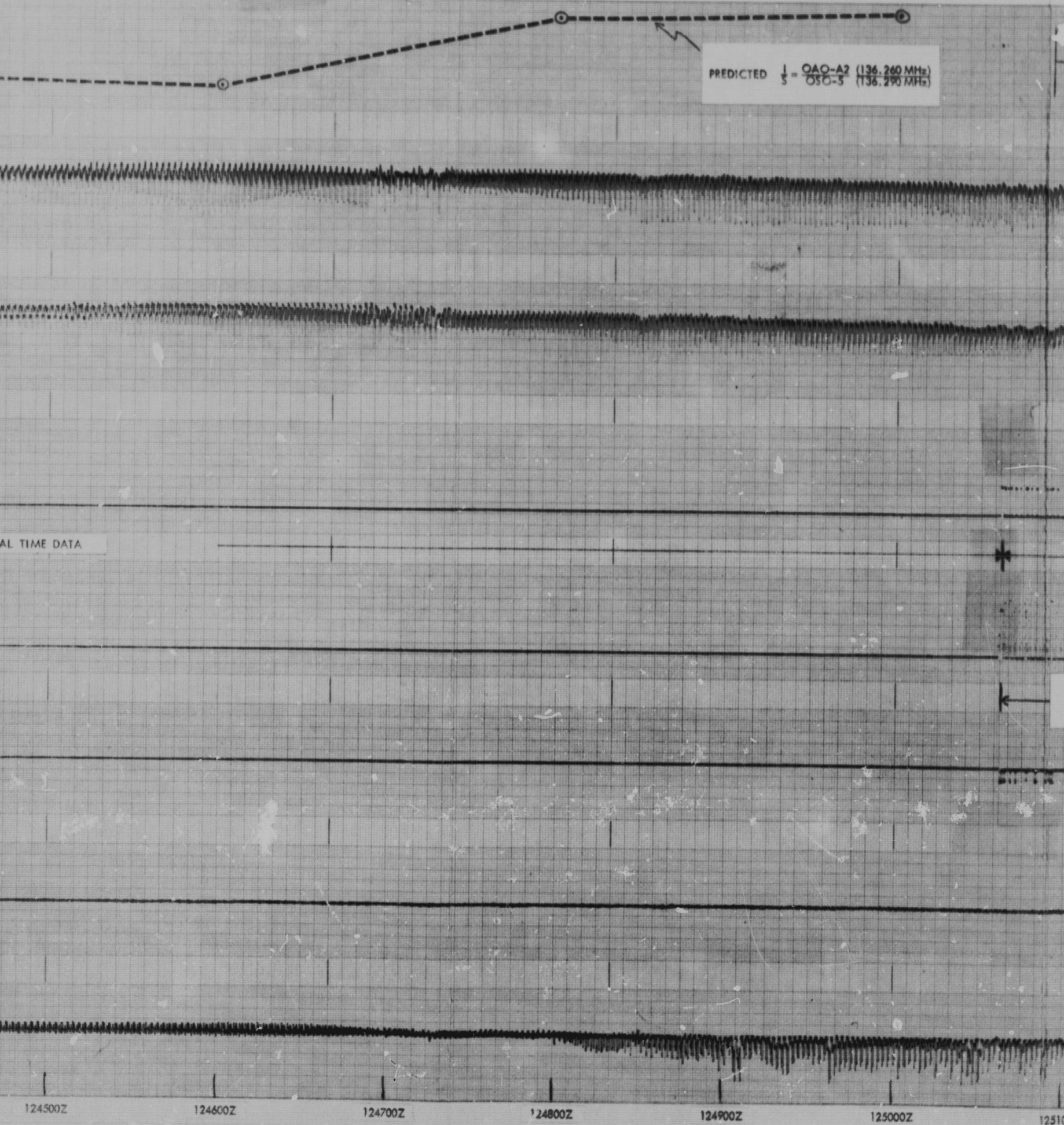
FOLDOUT FRAME #3

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FOLDOUT FRAME #1

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR.



EXOLDOUT FRAME #2

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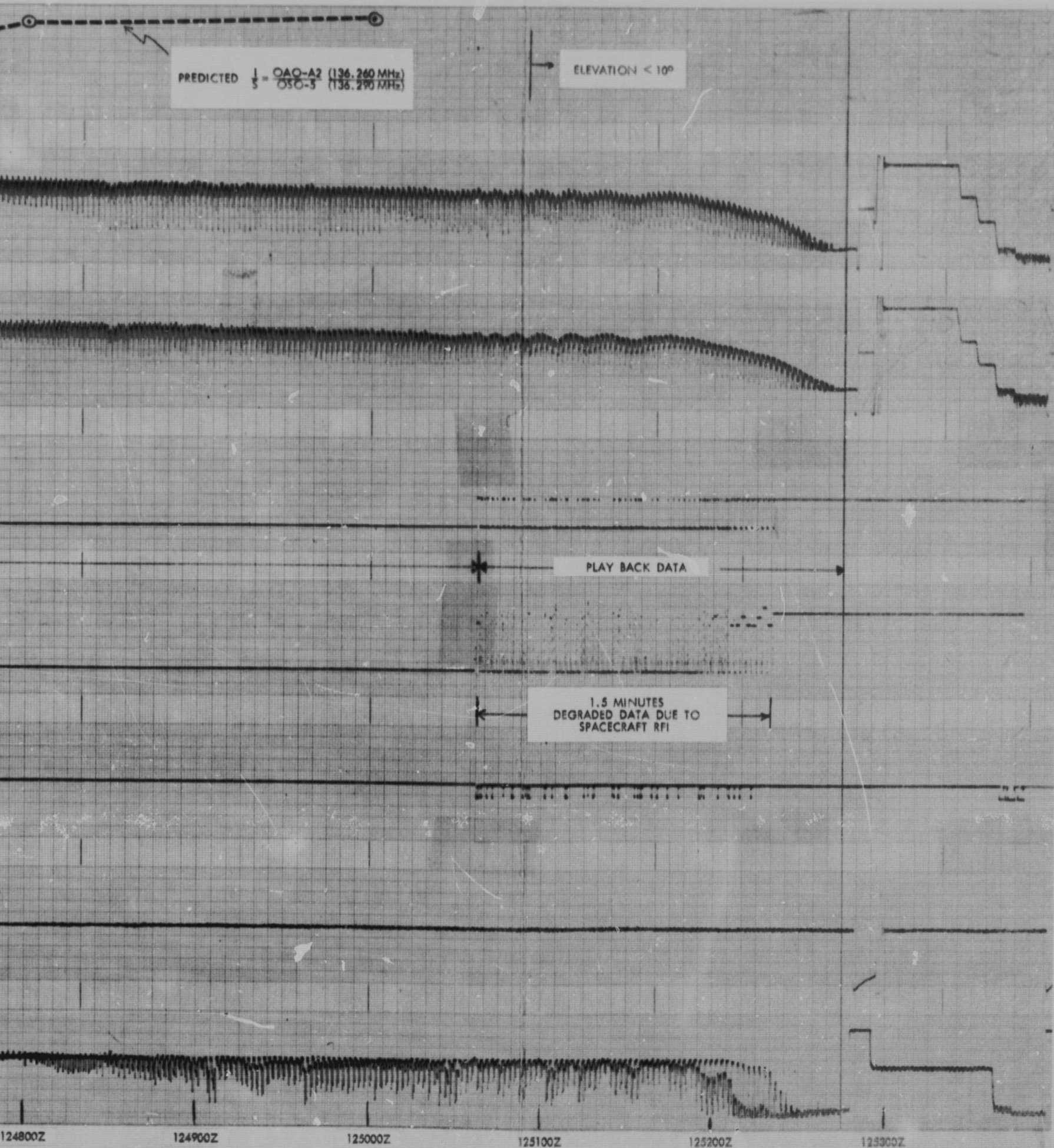


Figure 7. IPD Tape Evaluation Analysis for Mojave OSC-5(r) . Jpe No. 12

FOLDOUT FRAME # 2

FOLDOUT FRAME # 3

A similar incident also occurred for one minute, at the end of the 9-minute long OSO-5 tape No. 40 from the Orroral station, when both receiver channels "A" and "B" were inadvertently phase locked to the interfering OAO-A2 signal. At one time, a 30 kHz signal appeared on the data track (observed by spectrum analyzer) which is the difference frequency between the OSO-5 and OAO-A2 carrier frequencies.

Figure 6, corresponding to the OSO-5 Santiago tape No. 39, reveals a similar situation wherein the telemetry receiver "B" channel was inadvertently phase locked to the OAO-A2 signal; whereas, channel "A" was locked to the OSO-5 signal being tracked. Both the "real-time" and "playback" OSO-5 data were lost at this time, for about a 2.5 minute interval, at the beginning of the pass; a total of 10.5 minutes of data was either lost, or degraded, due to spacecraft RFI, during this 11-minute pass.

The predicted OAO-A2 interference level reduced to a value close to the $I/S = -20$ db threshold, at about 210900Z, with a corresponding reduction in interference measured by the Frame Sync Correlator output. GEOS-2, on an adjacent-channel 136.320 MHz carrier frequency, was predicted to cause interference with OSO-5 at 211200Z; there was a corresponding increase in the OSO-5 Frame Sync Correlator output channel at that time.

Mojave OSO-5 tape No. 12 (Figure 7) is interesting from two standpoints. First, even though the predicted interference-to-signal ratio was high above the -20 db interference threshold level, the OAO-A2 transmission did not interfere with the OSO-5 "real-time" data transmission. However, the moment the OSO-5 wide band "playback" data began transmitting at 125037Z, there was a corresponding step increase in interference as simultaneously monitored by the IPD tape evaluation processor averaged frame sync correlator and bit-sync slip-page channels (Figure 7). Consequently, 1.5 minutes of a 2-minute "playback" dump were significantly degraded, or lost, at the end of the pass.

C. STADAN Station RFI Report Analysis

The STADAN ground stations, while taking spacecraft telemetry data, and observing interferometer-type minitrack meridian crossings, also monitor the received spacecraft signal level as well as RFI that may be present during the pass. A separate teletype message, of each RFI event, has been reported by the stations; the weekly summary reports (Reference 6), generated from the daily teletype-messages, were received, and only spacecraft-type RFI events, described as such in the summary reports, were counted.

The station RFI reports were analyzed from two aspects: first, the total number of 136 MHz spacecraft RFI events occurring within a 7-month period, were graphed versus carrier frequency to reveal interference loading within the band; second, the average percentage of spacecraft RFI was computed, in terms of the total minutes of recorded data, for a given period of time. The total number of minutes of telemetry data, recorded by the STADAN stations, was obtained from the Reference 7 Weekly Reports.

The station RFI reports were graphed into two groups; the first group covering the 136.0 MHz to 136.5 MHz region, and the second covering the 136.5 MHz to 138.0 MHz portion of the band. The total number of reported spacecraft RFI events, in both Figures 8 and 9, contain only RFI identified by the stations as being either confirmed interference from another spacecraft, or interference "highly suspected" by station personnel as originating from another spacecraft. For example, slightly over 300 such interference events were reported for the AIMP-E operations (136.11 MHz) for a 7-month period (Figure 8).

Figure 8 shows that the lower 0.5 MHz portion (136.0-136.5 MHz) of the space research band is more heavily populated with spacecraft-type RFI than the upper 1.5 MHz (136.5-138.0 MHz) portion of the band. For instance, 60.5% of the spacecraft RFI events occurred within the one-half megahertz 136.0-136.5 MHz region; whereas Figure 9 shows that only 39.5% of the spacecraft RFI events occurred within the 136.5-138.0 MHz region—a bandwidth, 3 times as wide. The data in Figures 8 and 9 includes station reports for both telemetry and minitrack operations.

To compute the average percentage spacecraft RFI, a detailed analysis was made of four typical spacecraft—(AIMP-E, IMP-5, OSO-5, and ERS-28)—to determine the average level of spacecraft RFI observed in STADAN operations for these spacecraft. The detailed analysis is given in Tables I through IV, inclusive; a tabulated summary of the results is given in Table V.

The AIMP-E spacecraft (No. 7, Figure 8) had the largest number of reported spacecraft RFI events, for the 66 frequencies in the 136 MHz band, yet AIMP-E shows less than 1% spacecraft RFI when normalized to the total minutes of telemetry data recorded for that spacecraft. On the other hand, spacecraft including IMP-5, (No. 5, Figure 8) and OSO-5 (No. 20, Figure 8), show over 2% spacecraft RFI for correspondingly fewer RFI events. Furthermore, ERS-28 (No. 56, Figure 9) shows only 0.24% spacecraft RFI for the 136.84 MHz telemetry data channel, but over 6% reported spacecraft interference for Minitrack Operations.

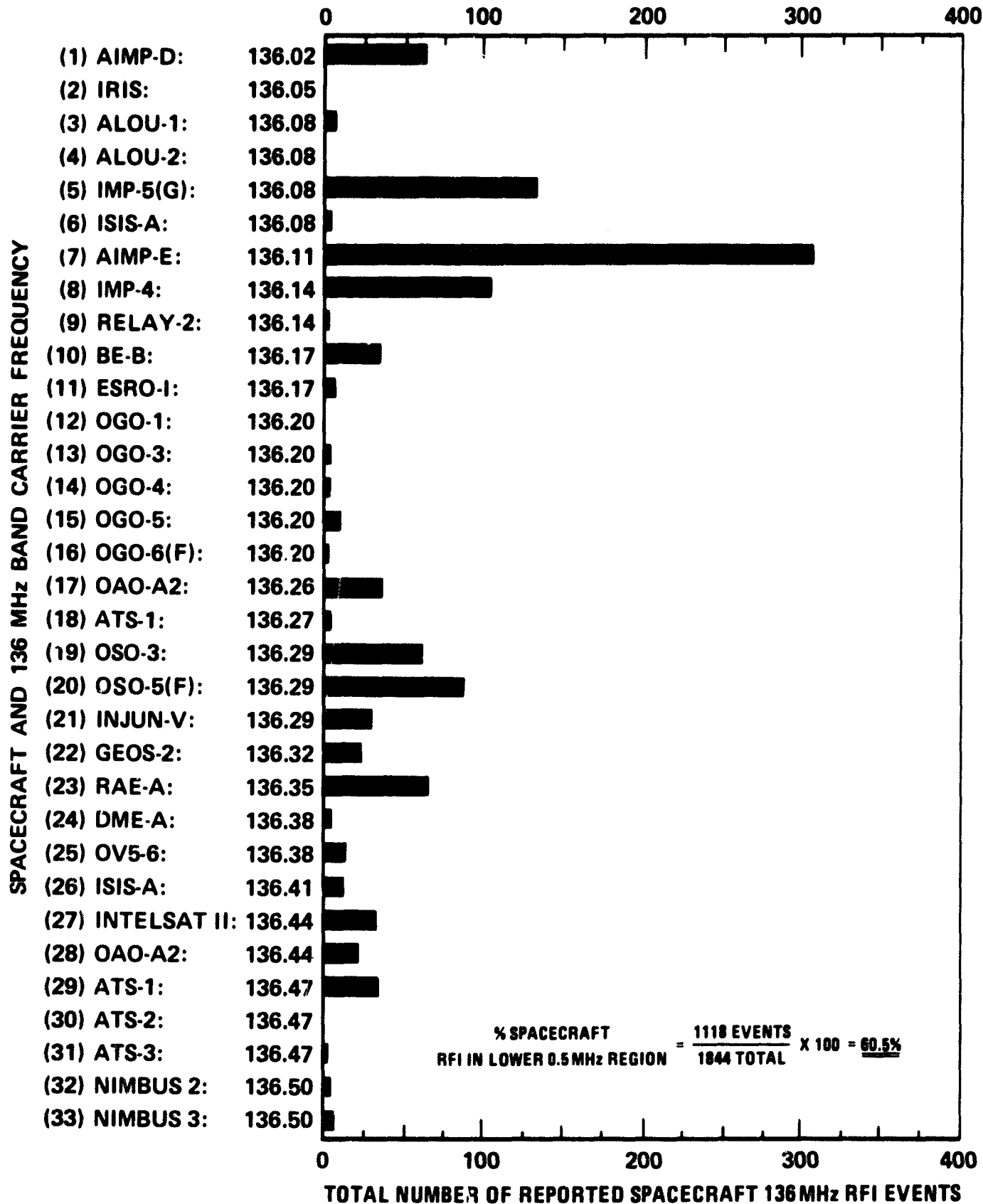


Figure 8. STADAN-Reported Spacecraft RFI Events in 136.0-136.5 MHz Region for January-July 1969 (7 Months)

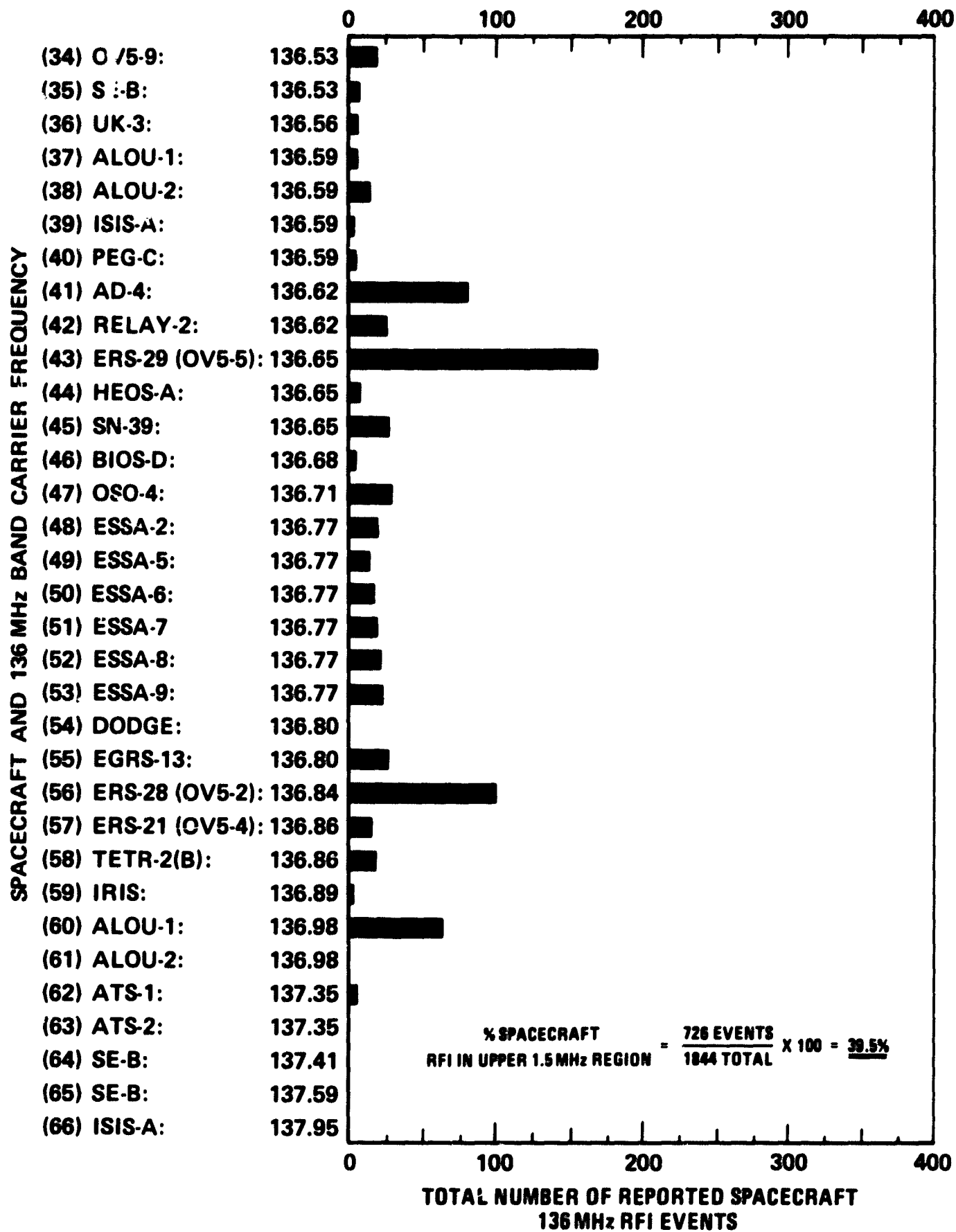


Figure 9. STADAN-Reported Spacecraft RFI Events in 136.50-138.00 MHz Region for January-July 1969 (7 Months)

Table I
STADAN Station-Reported Spacecraft RFI for AIMP-E
(3-Week Period)

Date		STADAN Station	Station-Reported RFI Start-Stop Time (HH MM SS)	Spacecraft RFI Event Duration (MM SS) 136 MHz Telemetry (TLM)
(1) 1-1-69	1st Week in Jan. '69	JOBURG	184014Z-194100Z	6046
(2) 1-1-69		SNTAGO	-	†
(3) 1-5-69		ALASKA	151600Z-151725Z	0125
(4) 2-1-69	1st Week in Feb. '69	ALASKA	112240Z-112420Z	0140
(5) 2-1-69		FT MYRS	011455Z-011600Z	0105
(6) 2-1-69		FT MYRS	230300Z-230500Z	0200
(7) 2-2-69		ALASKA	093330Z-094245Z	0915
(8) 2-2-69		JOBURG	203830Z-204900Z	1030
(9) 2-3-69		ALASKA	115220Z-115500Z	0240
(10) 2-3-69		ALASKA	-141240Z	†
(11) 2-3-69		JOBURG	201200Z-202145Z	0945
(12) 2-3-69	1st Week in Mar. '69	FT MYRS	025000Z-025955Z	0955
(13) 2-3-69		FT MYRS	081000Z-081900Z	0900
(14) 2-5-69		JOBURG	222500Z-222600Z	0100
(15) 2-6-69		SNTAGO	090810Z-091400Z	0550
(16) 2-7-69		SNTAGO	072600Z-073200Z	0600
(17) 3-1-69		ALASKA	055830Z-060300Z	0430
(18) 3-1-69		ALASKA	135910Z-140330Z	0420
(19) 3-2-69		ALASKA	101700Z-101900Z	0200
(20) 3-2-69		JOBURG	182800Z-185000Z	2200
(21) 3-2-69		JOBURG	203600Z-204000Z	0400
(22) 3-3-69		ALASKA	082800Z-083230Z	0430
(23) 3-3-69		JOBURG	014340Z-014430Z	0050
(24) 3-4-69		FT MYRS	044800Z-045500Z	0700
(25) 3-4-69		MADGAR	170720Z-170920Z	0200
(26) 3-5-69		FT MYRS	045800Z-050800Z	1000
(27) 3-7-69		ORORAL	134940Z-135347Z	0407
(28) 3-7-69	ORORAL	211900Z-213500Z	1600	
Total Observed Spacecraft RFI -				212.1 minutes
Average AIMP-E RFI Duration - 8.2 mins/RFI event				
Average % Spacecraft RFI observed - $\frac{(8.2 \text{ mins/RFI event}) (28 \text{ RFI events})}{29,643 \text{ mins TLM data taken}} \times 100 = 0.77\%$				
in AIMP-E Operations				

† RFI event occurred; duration not reported.

Table II
STADAN Station-Reported Spacecraft RFI for IMP-5 (1-Week Period)

Date		STADAN Station	Station-Reported RFI Start-Stop Time (HH MM SS)	Spacecraft RFI Event Duration (MM SS) 136 MHz Telemetry (TLM)
(1) 6-24-69	1st Day	JOBURG	113000Z-114800Z	1800
(2) 6-24-69		SNTAGO	154900Z-155130Z	0230
(3) 6-25-69	2nd Day	ALASKA	212000Z-213100Z	1100
(4) 6-25-69		JOBURG	071400Z-071555Z	0155
(5) 6-25-69		JOBURG	095250Z-095310Z	0020
(6) 6-25-69		JOBURG	110505Z-111400Z	0855
(7) 6-26-69	3rd Day	ORORAL	013106Z-014024Z	0918
(8) 6-26-69		JOBURG	103600Z-104500Z	0900
(9) 6-27-69	4th Day	ALASKA	135125Z-140515Z	1450
(10) 6-27-69		ROSMAN	145700Z-150800Z	1100
(11) 6-27-69		ROSMAN	151700Z-152500Z	0800
(12) 6-27-69		ROSMAN	160400Z-161200Z	0800
(13) 6-27-69		ROSMAN	164900Z-165200Z	0300
(14) 6-27-69		ROSMAN	180000Z-180600Z	0600
(15) 6-27-69		ROSMAN	154740Z-155650Z	0910
(16) 6-27-69		ROSMAN	161900Z-162700Z	0800
(17) 6-27-69	5th Day	JOBURG	083000Z-084156Z	1156
(18) 6-28-69		JOBURG	084410Z-085520Z	1110
(19) 6-28-69	Day	MADGAR	134510Z-141200Z	2750
(20) 6-29-69	6th Day	JOBURG	085700Z-090900Z	1200
(21) 6-29-69	Day	MADGAR	073710Z-074400Z	0650
(22) 6-30-69	7th Day	JOBURG	082200Z-082600Z	0400
(23) 6-30-69		QUITOE	141000Z-141040Z	0040
(24) 6-30-69		SNTAGO	161300Z-161750Z	0450
(25) 6-30-69		SNTAGO	162440Z-163015Z	0535
(26) 6-30-69		MADGAR	073710Z-074400Z	0650
(27) 6-30-69		MADGAR	124500Z-124800Z	0300
Total Observed Spacecraft RFI - 223.7 minutes				
Average IMP-5 RFI Duration - 8.3 mins/RFI event				
Average % Spacecraft RFI observed in IMP-5 Operations - 2.05%*				

* $\frac{(8.3 \text{ mins./RFI event}) (27 \text{ RFI events})}{10,913 \text{ mins. TLM data recorded}} \times 100 = 2.05\%$

Table III
STADAN Station-Reported Spacecraft RFI for OSO-5 (3-Week Period)

Date	STADAN Station	Station-Reported RFI Start-Stop Time (HH MM SS)	Spacecraft RFI Event Duration (MM SS) 136 MHz Telemetry (TLM)
(1) 1-22-69	JOBURG	171900Z-172400Z	0500
(2) 1-22-69		205240Z-	†
(3) 1-25-69		At 152000Z	†
(4) 1-26-69		At 162000Z	†
(5) 1-27-69		-	†
(6) 1-28-69	ORORAL	102840Z-103000Z	0120
(7) 1-28-69		121100Z-121830Z	0730
(8) 1-28-69		124900Z-130100Z	1200
(9) 1-29-69		230100Z-231250Z	1150
(10) 1-31-69		-	†
(11) 1-31-69	FT MYRS	105000Z-105400Z	0400
(12) 2-1-69	SNTAGO	210251Z-211400Z	1109
(13) 2-3-69	ORORAL	-	†
(14) 2-3-69	FT MYRS	070900Z-072200Z	1300
(15) 2-4-69	SNTAGO	172253Z-173400Z	1107
(16) 2-6-69	ORORAL	-	†
(17) 2-8-69	ORORAL	-	†
(18) 2-9-69	ORORAL	-	†
Total Observed Spacecraft RFI - 76.9 minutes			
Average OSO-5(F) RFI Duration - 8.6 mins/RFI event			
Average % Spacecraft RFI observed in OSO-5(F) Operations - 2.27%*			

* $\frac{(3.6 \text{ mins./RFI event}) (18 \text{ RFI events})}{6,819 \text{ mins. TLM data recorded}} \times 100 = 2.27\%$

† RFI event occurred; duration not reported.

Table IV
STADAN Station-Reported Spacecraft RFI for ERS-28 (3-Week Period)

Date	STADAN Station	Station-Reported RFI Start-Stop Time (HHMMSS)	Spacecraft RFI Event Duration (MMSS)	
			136 MHz Telemetry (TLM)	Minitrack (M/T)
(1) 1-1-69	SNTAGO	141122Z-142000Z	0838	
(2) 1-1-69	SNTAGO	155600Z-160300Z	0700	
(3) 1-3-69	JOBURG	030200Z-081100Z		0900
(4) 1-4-69	SNTAGO	124400Z-130400Z		2000
(5) 1-5-69	QUITOE	010800Z-014000Z		3200
(6) 1-6-69	MADGAR	- -		†
(7) 2-1-69	SNTAGO	113500Z-115700Z		2200
(8) 2-1-69	MADGAR	025000Z-032000Z		3000
(9) 2-3-69	FT MYRS	134400Z-135200Z	0800	
(10) 2-3-69	FT MYRS	140800Z-141200Z	0400	
(11) 2-7-69	JOBURG	- -		†
(12) 3-3-69	MADGAR	- -		†
(13) 3-4-69	QUITOE	- -		†
(14) 3-5-69	MADGAR	170530Z-171800Z		1230
(15) 3-6-69	LIMA PU	- -		†
Total Observed Spacecraft RFI -			27.5 minutes	125.5 minutes
Average ERS-28 RFI Duration -			6.9 mins/RFI event	20.9 mins/RFI event
Average % Spacecraft RFI observed in ERS-28 Operations -			0.24%*	6.09%**

* $(6.3 \text{ mins./RFI event}) (4 \text{ RFI events}) / 11,429 \text{ mins. TLM data recorded} \times 100 = 0.24\% \text{ for Telemetry.}$

** $(20.9 \text{ mins./RFI event}) (11 \text{ RFI events}) / (16.8 \text{ mins. per M/T pass}) (225 \text{ passes}) \times 100 = 6.09\% \text{ for Minitrack.}$

† RFI event occurred; duration not reported.

Table V
Summary of Typical Station-Reported Spacecraft Interference in 136 MHz Band

Spacecraft	Observation Period (Weeks)	Total Number of Spacecraft RFI Events Reported	Total Observed RFI (Minutes)	Average Spacecraft RFI Event Duration (Minutes/Event)	Minutes of 136 MHz Data Recorded		Average Percentage 136 MHz Spacecraft RFI
					Telemetry	Minitrack	
AIMP-E	3	28	212.1	8.2	29,643	—	0.77%
IMP-5	1	27	223.7	8.3	10,913	—	2.05%
OSO-5	3	13	76.9*	8.6	6,819	—	2.27%
ERS-28	3	4	27.5	6.9	11,429	—	0.24%
ERS-28	3	11	125.5	20.9	—	3,780	6.09%

*Playback and Real-time included

IV. CORRELATION OF PREDICTED, REPORTED, AND TAPE-OBSERVED SPACECRAFT RFI

All fourteen (14) OSO-5(F) analog tapes, examined by the IPD contained interference that was either CLEARLY IDENTIFIED as spacecraft-type RFI, or placed in the category of "suspected" spacecraft RFI. Table VI is a summary of the STADAN-station reported, the ADD-predicted, and the corresponding IPD-observed interference for the fourteen (14) OSO-5(F) sample tapes; there is excellent agreement between all three categories.

Eight of the strip-chart analog tapes, corresponding to station magnetic tape Nos. 17, 18, 27, 32, 28, 40, 45, and 39, listed in Table VII, show good time correlation between the predicted, the reported and the analog-tape observed start/stop times for the spacecraft-type RFI. For instance, Table VII shows that the start/stop times for the predicted (and observed values) agree within 0 to 4 minutes that corresponds to an accuracy commensurate with the accuracy of the Brouwer orbital elements utilized in the IBM 360 program, in turn used to predict spacecraft RFI.

The remaining six (6) strip-chart tapes, corresponding to station magnetic tape Nos. 07, 08, 30, 26, 12, and 38, listed in Table VI, show four (4) predicted and IPD-observed RFI events for OSO-5(F) that were "not reported" by the STADAN stations, and two (2) spacecraft type RFI events in the "not predicted" category.

The "not predicted" RFI events are explained as follows: first, one IPD-observed RFI event, existing for only one (1) minute, on tape No. 07, could have been missed by the computer since the prediction printout times are at 2-minute intervals; second, the IPD-observed spacecraft-type RFI event, on tape No. 26, occurred at an elevation angle, of less than 10° , that is, below the minimum cutoff elevation angle used in the prediction computer program.

There is evidence in the Table VI listing that the STADAN stations have become fairly adept at identifying spacecraft-type RFI; for instance, the station correctly identified eight (8) out of twelve (12) interfering spacecraft that were predicted to cause interference with OSO-5(F). Furthermore, the station reported interference start/stop times (see Table VII listing) are also in reasonable agreement with the ADD-predicted and the IPD-observed start/stop times.

The predictions in the Table VI listing show that the OAO-A2, INJUN-5, and GEOS-2 spacecrafts were involved in interference events with OSO-5(F) at various times, as observed by the IPD, in the fourteen OSO-5(F) sample tapes. Table VIII lists the spacecraft, and corresponding transmitter parameters, inputted in the OSO-5(F) prediction program.

Table VI
Comparison of STADAN Reported, ADD Predicted, and IPD Observed
OSO-5 Spacecraft RFI Start/Stop Times

STADAN Station	Tape No.	STADAN Reported (Daily Report)					ADD Predicted					IPD Observed		
		Date	Start (HH MM)	Stop (HH MM)	Suspected S/C	Max. AGC Level (-dbm)	Start (HH MM)	Stop (HH MM)	Interfering S/C	Worst I/S (db)	Time (HH MM)	AGC (-dbm)	Start (HH MM)	Stop (HH MM)
(1)MOJAVE	07	1/26/69	1620Z	—	OA0-A2 GEOS-2	88	—	—	Not Predicted*	—	—	—	1623Z	1634Z
(2)SNTAGO	17	1/27/69	0059Z	—	OA0-A2	NR	0102Z	—	OA0-A2	-18.1	0102Z	92.2	0102Z	0103Z
(3)SNTAGO	18	1/27/69	0240Z	—	OA0-A2	84	0244Z	0250Z	OA0-A2	-13.1	0244Z	91.4	0243Z	0251Z
(4)MOJAVE	08	1/27/69	Not Reported			87	1252Z	—	Injun-5	-17.6	1252Z	85.9	1252Z	1257Z
(5)FT MYRS	30	1/28/69	Not Reported			88	0934Z	—	GEOS-2	-9.9	0934Z	88.8	0931Z	0932Z
(6)ORORAL	26	1/28/69	1029Z	1030Z	OA0-A2	NR	—	—	Not Predicted**	—	—	—	1029Z	1031Z
(7)ORORAL	27	1/28/69	1211Z	1218Z	OA0-A2	NR	1214Z	1216Z	OA0-A2	-14.1	1214Z	92.4	1214Z	1216Z
(8)MOJAVE	12	1/28/69	Not Reported			85	1244Z	1250Z	OA0-A2	+1.2	1248Z	87.2	1250Z	1252Z
(9)FT MYRS	32	1/28/69	1249Z	1301Z	OA0-A2	90	1252Z	1258Z	OA0-A2	-1.4	1254Z	86.9	1250Z	1258Z
(10)SNTAGO	28	1/29/69	2301Z	2313Z	OA0-A2	NR	2304Z	2310Z	OA0-A2	-8.4	2304Z	91.1	2300Z	2312Z
(11)ORORAL	40	1/31/69	1011Z	EOP	OA0-A2	NR	1014Z	1018Z	OA0-A2	-11.4	1014Z	92.6	1018Z	1020Z
(12)FT MYRS	45	1/31/69	1050Z	1054Z	OA0-A2 GEOS-2 Injun-5 OSO-3	92	1054Z	1100Z	OA0-A2	-15.1	1054Z	89.6	1052Z	1059Z
(13)SNTAGO	38	1/31/69	Not Reported			83	1924Z	—	OA0-A2	-14.6	1924Z	91.6	1924Z	1930Z
(14)SNTAGO	39	2/01/69	2103Z	2114Z	OA0-A2	83	2106Z	2112Z	OA0-A2 GEOS-2	17.5 17.2	2112Z	90.7	2103Z	2113Z

*RFI lasted for less than 2 minutes.

**OSO-5 elevation angle < 10°

NR = Not Reported

Table VII
Correlation of Predicted, Observed, and STADAN-Reported
Start/Stop Times for Spacecraft-Type RFI

OSO-5 Magnetic Tape No.	STADAN Station	Time Spacecraft-Type RFI Is Present							
		Start Times				Stop Times			
		ADD Predicted (HH MM)	IPD Observed (HH MM)	Start Time Difference, $ \Delta t $ * Start (minutes)	STADAN Reported (HH MM)	ADD Predicted (HH MM)	IPD Observed (HH MM)	$ \Delta t $ * Stop (minutes)	STADAN Reported (HH MM)
17	SNTAGO	0102Z	0102Z	00	0059Z	—	0103Z	—	—
18	SNTAGO	0244Z	0243Z	01	0240Z	0250Z	0251Z	01	—
27	ORORAL	1214Z	1214Z	00	1211Z	1216Z	1216Z	00	1218Z
32	FT MYRS	1252Z	1250Z	02	1249Z	1258Z	1258Z	00	1301Z
28	SNTAGO	2304Z	2300Z	04	2301Z	2310Z	2312Z	02	2313Z
40	ORORAL	1014Z	1018Z	04	1011Z	1018Z	1020Z	02	EOP
45	FT MYRS	1054Z	1052Z	02	1050Z	1100Z	1059Z	01	1054Z
39	SNTAGO	2106Z	2103Z	03	2103Z	2112Z	2113Z	01	2114Z

* $|\Delta t|$ = |Predicted Time (HH MM) - Observed Time (HH MM)| minutes. EOP = End of Pass

Table VIII
Spacecraft Parameters Inputted to OSO-5(F) Spacecraft
RFI Prediction Program

Tracking Spacecraft	Interfering Spacecraft	Spacecraft Transmitter Characteristics* used in the RFI Prediction Program			
		RF Power (watts)	Carrier Frequency (MHz)	Bandwidth (kHz) Real-Time Mode	Bandwidth (kHz) Playback Mode
OSO-5(F)	—	0.57	136.290	10	40
—	OA0-A2	1.60	136.260	40	—
—	INJUN-5	0.25	136.290	30	—
—	GEOS-2	0.40	136.320	20	—
—	OSO-3	0.57	136.290	10	40**

*Assumes an Isotropic-type spacecraft antenna

**OSO-3 wideband "playback" mode (7.2 K b/s bit rate) was inoperative; only 400 b/s "real-time" mode operated

The STADAN antenna used during the recorded pass was used in the prediction program for determining the I/S ratios.

V. OSO-5(F) 136 MHz TELEMETRY DATA LOST OR DEGRADED

The Information Processing Division carefully examined the fourteen (14) selected OSO-5(F) station magnetic tape recordings, and resulting analog strip charts and evaluation results to determine the amount of lost and degraded data. The resulting lost and degraded data expressed in minutes, was then identified with both the "real-time" and "playback" modes. These modes were then further identified with spacecraft-type RFI, and interference from other sources, including atmospheric disturbances, etc. The following criteria were utilized to make this identification:

- Averaged frame sync bit errors counted at correlator output to determine average PCM bit error probability
- Length of time interference was present determined from analog strip charts reproduced from station magnetic tapes
- Spacecraft-type RFI detected in "raw" magnetic tape data using 1) spectrum analyzer, to identify bit rates; 2) using AGC's and S+N variations to observed interference and varying S/N ratios; and 3) using oscilloscope and viscorder to identify interference-intermodulation waveforms.
- Interference-to-Signal threshold of $I/S \geq -20$ db used to determine if spacecraft-type interference was predicted.

The minutes of lost and degraded data, resulting only from spacecraft-type RFI, for both "real-time" and "playback" modes, was then tabulated (Table IX) versus the actual recorded telemetry data (in minutes) for the whole pass. The subsequent "lost" and "degraded" data percentages were then expressed for both "real-time" and "playback" modes (also see Figure 10).

Considering only the effects of spacecraft-type RFI, the percentages of lost and degraded OSO-5(F) "real-time" and "playback" data per spacecraft RFI averaged out as shown in Tables IX and X.

It is thus seen that the OSO-5(F) "playback" data is more seriously affected, by interference from other spacecraft, than the "real-time" data.

The average bit error probability, P_e , for the fourteen (14) OSO-5(F) spacecraft RFI tapes, was then determined from the percentage of recovered frame sync words (FOE), with zero errors, and the expressions:

$$FOE \approx (1 - n P_e)$$

where n = number of bits in each frame sync word, 16 for OSO spacecraft.

Table IX
IPD Analysis of OSO-5(F) Magnetic Tapes Containing Lost or Degraded Data

STADAN Station	Tape No.	Actual Recording Interval		Lost/Degraded Data Due to Interference from Other Spacecraft								Average Bit Error Probability	
				Mins Lost		Mins Degraded		% Lost					
		RT (mins)	PB (mins)	RT	PB	RT	PB	RT	PB	RT	PB	RT*	PB*
(1)MOJAVE	07	11.0	2.0	0.3	1.0	1.0	1.0	2.7	50.0	9.1	50.0	10 ⁻³	10 ⁻²
(2)SNTAGO	17	6.5	5.5	0	0	0	1.0	0	0	0	18.2	10 ⁻²	10 ⁻³
(3)SNTAGO	18	5.5	5.5	0.2	2.5	3.5	3.0	3.6	45.0	63.6	54.5	10 ⁻²	10 ⁻²
(4)MOJAVE	08	10.5	2.0	0	0	0	1.0	0	0	0	50.0	10 ⁻⁵	10 ⁻²
(5)FT MYRS	30	8.0	5.5	0	0	0	0.5	0	0	0	9.1	10 ⁻⁵	10 ⁻⁴
(6)ORORAL	26	12.0	0	1.0	—	1.0	—	8.3	—	8.3	—	10 ⁻²	—
(7)ORORAL	27	8.0	0	0	—	2.0	—	—	—	25.0	—	10 ⁻³	—
(8)MOJAVE	12	10.0	2.0	0	1.0	0	1.0	0	50.0	10.0	50.0	10 ⁻⁵	10 ⁻¹
(9)FT MYRS	31	8.5	5.5	0	2.0	2.0	3.5	0	36.3	23.4	63.8	10 ⁻²	10 ⁻¹
(10)SNTAGO	28	7.5	5.5	3.5	0.1	4.0	5.4	46.8	1.8	53.3	98.0	10 ⁻¹	10 ⁻²
(11)ORORAL	40	9.0	0	2.0	—	1.0	—	22.2	—	11.1	—	10 ⁻³	—
(12)FT MYRS	45	6.5	6.5	0	0.5	1.0	6.0	0	7.8	15.4	92.3	10 ⁻²	10 ⁻²
(13)SNTAGO	38	5.5	6.0	0	0	0	2.0	0	0	0	33.3	10 ⁻⁴	10 ⁻⁴
(14)SNTAGO	39	5.5	5.5	1.0	2.0	4.0	3.5	18.2	36.4	72.8	63.7	10 ⁻²	10 ⁻¹
Total Minutes		114.0	51.5	8.0	9.1	19.5	27.9	7.0% Average	17.7% Average	17.1% Average	54.2% Average	1 x 10 ⁻² Average	3 x 10 ⁻² Average

*"Real-Time" average bit error probability includes degrading influences from all sources, i.e., other spacecraft, atmospheric disturbances, fading signal levels at low elevation angles, etc. "Playback" average bit error probability includes only effects of interference from "other spacecraft." RT = Real-Time; PB = Playback.

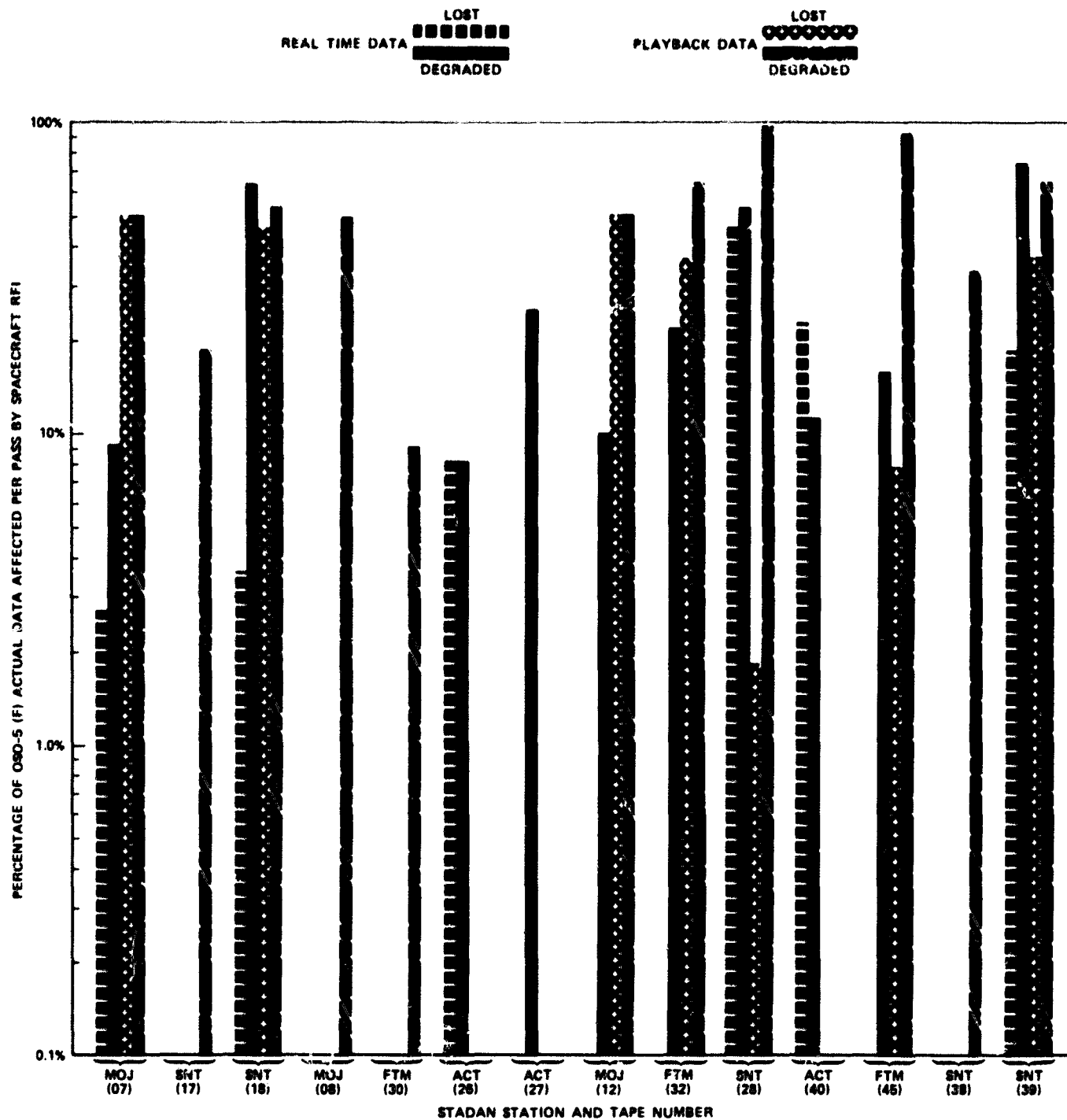


Figure 10. Percentage Real-Time and Playback Data Affected By Spacecraft RFI in Fourteen (14) OSO-5(F) Passes

Table X
OSO-5(F) Real-Time/Playback Lost/Degraded Data Due to
Spacecraft RFI, in 14 Tapes

	Real-Time	Playback
Average Lost Data	7.0%	17.7%
Average Degraded Data	17.1%	54.2%

The standard theoretical bit error probability curve for gaussian noise distribution and "matched" filter detection was then used to relate P_e and normalized signal-to-noise ratios (db).

The resulting "real-time" average bit error probability includes degrading influence from ALL SOURCES, i.e., other spacecraft, atmospheric disturbances, fading signals at low elevation angles, etc., whereas the "playback" average bit error probability includes ONLY effects of interference from "other spacecraft."

The "playback" average PCM bit error probability was significantly degraded, due to spacecraft RFI, in a number of the fourteen OSO-5(F) tapes (see right-hand column, Table IX). For instance, the average "playback" bit error probability for all tapes with "playback" data, is 3×10^{-2} . This represents a degradation of over three orders of magnitude, or a corresponding signal-to-noise ratio change of 7db in the data bandwidth, compared to the "quiet," interference-free, average "fidelity" reference level of 2.5×10^{-5} found in reference 8.

The "real-time" PCM bit error probability, for all fourteen (14) OSO-5(F) magnetic tapes, averaged 1×10^{-2} due to degrading influences from all sources. Separation of spacecraft RFI effects from all other noise sources for the "real-time" bit error probability is practically impossible for the tapes analyzed.

Table XI tabulates the lost and degraded minutes of data in the fourteen spacecraft RFI tapes found in the one week sample for OSO-5(F) along with the scheduled pass(s) durations for the week.

Averaged over the total number of 173 data tapes for the one week sample, 0.53% of the "real-time" data are lost due to spacecraft interference and 1.29% of the data are degraded. In addition, 1.3% of the "play-back" data are lost due to spacecraft interference; 3.99% of the data are degraded due to spacecraft interference.

Table XI
Summary of OSO-5(F)* Lost and Degraded Data Due to Spacecraft
RFI for One Week Sample of 173 Tapes

Data Type	No. of Passes Per Day	Average Duration of Pass (minutes)	Total Scheduled Per Week (minutes)	Total Spacecraft RFI Per Sample Week		Average Effect of S/C RFI on OSO-5(F)	
				Lost (mins)	Degraded (mins)	Lost (%)	Degraded (%)
Real-Time	27	8	1512	8.0	19.5	0.53%	1.29%
Playback	20	5	700	9.1	27.9	1.30%	3.99%

*OAO-A2 is the main interfering source for the OSO-5(F) spacecraft.

VI. CONCLUSIONS

For the Orbiting Solar Observatory OSO-5(F) 136 MHz pulse-code modulation telemetry channel, it has been shown that a good correlation exists between the Advanced Development Division's spacecraft radio frequency interference (RFI) prediction program, the Information Processing Division's data processing analysis, and the STADAN station reports for spacecraft-type interference.

The ensuing spacecraft interference statistics, resulting from a thorough analysis of fourteen (14) typical OSO-5(F) station-recorded magnetic tapes, over a one week interval, and station interference reports, are summarized as follows:

- OSO-5(F) "playback" mode, utilizing a 14.4 kilobit/sec PCM bit rate, is more susceptible to adjacent-channel spacecraft-type interference than the 800 bit/sec "real-time" transmission mode.
- Considering only the degrading effects of spacecraft-type radio frequency interference in the one week sample, the average percentage of completely lost OSO-5(F) "real-time" data was 0.53%; whereas on the average, 1.29% of the data was seriously degraded normalized to a total of 173 data tape for the 1-week sample.
- PCM average bit error probability (3×10^{-2}), for the OSO-5(F) 136 MHz telemetry "playback" mode, degraded over three orders of magnitude from a "quiet" average quality reference of 2.5×10^{-5} . This represents a 7 db average signal-to-noise ratio degradation for 3.99% of the pass data recorded in 173 tapes for the sample week. The corresponding lost "playback" data due to spacecraft RFI is 1.3%.
- OAO-A2 was the main interfering source for the OSO-5(F) spacecraft during this seven-day sample.
- The average percentage of spacecraft-type interference, computed from STADAN stations reports, agrees with percentages derived from the processing of station data magnetic tapes. For instance, station-reported telemetry data statistics, for four typical STADAN-supported spacecraft, reveal an interference level, from other spacecraft, on the order of 1% or 2%; whereas the processed OSO-5(F) magnetic tape samples show that spacecraft-type interference level is the same order of magnitude for the "real-time" mode.
- STADAN-station interference reports for 66 telemetry channels, representing 48 spacecrafts, reveal that about 60% of the spacecraft-type interference occurs within the one-half megahertz bandwidth from 136.0-136.5 MHz, and 40% within the 1.5 MHz region from 136.5-138.0 MHz.

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